

Chardon-Mentor Road

85

LEVEL BOOK

744

INDEX

B. Ms.	CH. 5	3-7
X-Sections	"	9-46
Arch Bridge data	"	Pg 32-

9-13-22
Fair

B.M. LEVELS

Hanna
GRU

3

U.S.G.S. BM, 226 1235 03

1232.77

Frooz tablet N.E. Cor. C.T. Usher's

T.P. 1.54 1233 85 2.72 1232.31

house S.W. corner Court & Washington Sts.

T.P. 10.52 1239 09 5.28 1228.57

x N.E. Cor. Culv. W. of Meyer's.

T.P. 11.14 1249 64 0.59 1238.50

T.P. 11.35 1260 69 0.30 1249.34

T.P. 12.64 1273 16 0.17 1260.52

T.P. 11.74 1284 84 0.06 1273.10

T.P. 12.00 1296 84 9.00 1284.84

T.P. 6.57 1303 41 0.00 1296.84

T.P. 8.10 1309 03 2.48 1300.93

B.M. 5.94 1303.09

Nail in W. root 1st maple on Lt. Corp. line

T.P. 1.50 1297 82 12.71 1296.32

T.P. 1.46 1288 30 10.98 1286.84

T.P. 1.57 1277 21 12.66 1275.64

B.M. 3.84 1273.37

Nail in N.E. root 28" Apple (E. of Osborn's) Lt.

T.P. 0.65 1265 40 12.46 1264.75

T.P. 0.15 1253 17 12.38 1253.02

T.P. 10.95 1256 23 7.89 1245.28

B.M. 6.71 1249.52

S.E. cor. Rt. parapet.

³ Nails in N.W. root 36" Oak Lt.

T.P. 11.74 1267 97 0.00 1256.23

T.P. 11.48 1279 17 0.28 1267.69

T.P. 12.67 1291 18 0.66 1278.51

Sta.	B.S.	H.I.	F.S.	Elev.	
		1291.18			
T.P.	9.86	1301.00	0.04	1291.14	
T.P.	5.81	1305.30	1.51	1299.49	
^{m.} ^{s.} B.M.	9.30	1310.37	4.23	1301.07	Nail in S. root 24" Maple, at curve Rt.
T.P.	6.63	1315.38	1.62	1308.75	
T.P.	1.12	1307.81	8.69	1306.69	
B.M.	2.66	1306.87	3.60	1304.21	Spike in W. side 12" Maple Lt. (Wheat)
T.P.	6.38	1310.35	2.90	1303.97	
B.M.			5.98	1304.37	Nail in N.W. root 15" Hickory Lt. (E. of ^{house} Knopp)
T.P.	0.78	1306.18	4.95	1305.40	
T.P.	2.21	1297.11	11.28	1294.90	
T.P.	1.80	1289.84	9.07	1288.04	
B.M.			5.47	1284.37	Nail in N.E. root 40" Elm, Lt. W. side Ctr. Rd. (Stump?)
T.P.	2.78	1280.90	11.72	1278.12	
T.P.	1.60	1272.24	10.26	1270.64	
B.M.			2.11	1270.13	Nail in S. root 4" Chestnut Rt.
T.P.	1.00	1261.60	11.64	1260.60	
T.P.	0.31	1249.69	12.22	1249.38	
T.P.	0.81	1237.52	12.98	1236.71	
T.P.	1.83	1227.87	11.48	1226.04	
B.M.			3.56	1224.31	Nail in S.W. root 15" Apple Rt.
T.P.	0.46	1215.90	12.43	1215.44	
T.P.	2.36	1207.66	10.60	1205.30	

1207 66

B.M.

6.48 1201.18 spike in s. root 4' Chestnut Rt.

T.P. 0.77 1196 62 11.83 1195.85

T.P. 0.24 1184 89 11.97 1184.65

T.P. 0.11 1172 49 12.51 1172.38

T.P. 0.42 1160 29 12.62 1159.87

T.P. 0.53 1147 93 12.89 1147.40

T.P. 0.54 1135 49 12.98 1134.95

B.M.

2.55 1132.94

Bent

Spike in E. side 14" Apple E. of "Maple Rock" driveway

T.P. 9-20-22 12.55 1122.94

a.p. blue stone in roadway (Defaced by tractor)

B.M. 2.07 1135 01 1132.94

T.P. 0.07 1122 80 12.28 1122.73

T.P. 0.13 1110 39 12.54 1110.26

T.P. 2.35 1101 37 11.37 1099.02

B.M.

0.38 1000.99

110099

Nail with cap in W. root 20" Maple Rt.

T.P. 1.46 1094 42 7.41 1093.96

B.M.

3.39 1091.03

Nail with cap in s.w. root 19" Maple Rt.

T.P. 0.84 1089 24 6.02 1088.40

T.P. 0.30 1076 87 12.67 1076.57

T.P. 0.78 1064 70 12.95 1063.92

T.P. 0.10 1051 87 12.93 1051.77

T.P. 1.85 1042 36 11.36 1040.51

T.P. 0.11 1030 21 12.26 1030.10

B.M.

7.27 1022.94

Bottom of S.E. Corner board House to Ltr.

T.P. 0.28 1018 01 12.48 1017.73

1018 01

T.F. 001 1005 02 13.00 1005.01

T.F. 0.37 992 33 13.06 991.96

T.F. 0.61 979 95 12.99 979.34

T.F. 0.62 968 17 12.40 967.55

T.F. 0.29 955 57 12.89 955.28

T.P. 0.70 943 34 12.93 942.64

T.P. 1.68 932 15 12.87 930.47

B.M. 8.90 923.25

T.F. 10.74 942 35 0.54 931.61

T.P. 10.84 952 31 0.88 941.47

T.P. 12.35 964 12 0.54 951.77

T.P. 11.88 975 56 0.44 963.68

T.P. 12.59 987 55 0.60 974.96

T.P. 9.65 997 17 0.03 987.52

T.P. 10.04 1006 71 0.50 996.67

B.M. 2.68 1004.03

T.F. 10.81 1017 27 0.25 1006.46

T.P. 12.49 1029 50 0.26 1017.01

T.P. 12.84 1042 22 0.12 1029.38

T.P. 12.09 1054 29 0.02 1042.20

T.P. 12.22 1066 27 0.24 1054.05

T.P. 12.17 1078 19 0.25 1066.02

T.P. 11.82 1089 25 0.76 1077.43

T.P. 7.48 1096 20 0.53 1088.72

B.M. 2.39 1093.81

x on N.W. cor. Lt. wall to Arch Brg.

noon

Tinheaded tack N.E. Root 18" Maple Lt.

Tin Headed tack W. root 15" Maple Rt. front of empty house.

1096 20

T.P.	11.68	1102	57	5.36	1090.84
T.P.	12.38	1113	91	0.99	1101.53
T.P.	8.20	1119	85	2.26	1111.65
T.P.	8.63	1127	95	0.53	1119.32
J.M.				4.10	1123.79
T.P.	1.27	1116	72	12.50	1115.45
T.P.	0.74	1105	05	12.41	1104.31
T.P.	0.45	1093	02	12.48	1092.57
T.P.	0.40	1080	44	12.78	1080.04
T.P.	0.60	1068	36	12.68	1067.76
T.P.	0.31	1055	99	12.68	1055.68
T.P.	0.48	1044	86	11.61	1044.38
T.P.	1.23	1033	40	12.69	1032.17
J.M.				1.79	1031.61
T.P.	4.68	1029	42	8.66	1024.74
T.P.	11.21	1039	99	0.64	1028.78
T.P.	7.16	1042	77	4.38	1035.61
T.P.	1.34	1031	40	12.71	1030.06
J.M.				5.37	1026.03

Top large stone Lt.

Tin Headed tack N. root 36" Ash opposite Hickox est.

Tin Headed tack on W. root 15" Maple Rd.

Tin Headed tack in E. root 30" Maple at Lt. X rds.

Cross-Sections

Sta. B.S. H. I. F.S. Elev.

B.M. 6.83 1309.92 1303.09

0-100 10.3 1299.6

-200 11.2 1298.7

0 7.7 1302.2

1 5.1 04.8

2 3.8 06.1

3 6.5 03.4

4 8.9 01.0

5 10.5 99.4

6 12.2 97.7

T.P. 1.63 1298.98 12.57 1297.35

7 2.9 96.1

8 5.0 94.0

9 6.4 92.6

10 7.9 91.1

9-28-22
Fair-Hot

Hanna
Grou
Spohn

9

Nail in W. maple 'Lt. Sta 0-20

(x sections are actual rod readings)

+1.1 +0.3 -1.1 -0.2 0.0 -0.6 -1.2 -0.5 0.0 +0.6
 $\frac{6.6}{25} \frac{7.4}{17} \frac{8.8}{15} \frac{7.5}{5} \frac{7.7}{5} \frac{8.3}{6} \frac{8.9}{11} \frac{8.2}{13} \frac{7.7}{20} \frac{7.1}{25}$

+0.7 +0.8 +0.2 -1.7 -0.9 0.0 -0.6 -1.5 -0.3 +0.4
 $\frac{1.4}{25} \frac{1.3}{20} \frac{4.7}{16} \frac{4.8}{13} \frac{6.0}{9} \frac{5.1}{5} \frac{5.7}{7} \frac{6.6}{12} \frac{5.4}{14} \frac{4.7}{25}$

+0.8 +0.2 -1.2 -0.5 0.0 -0.5 -1.3 -0.2 +0.5
 $\frac{3.0}{25-19} \frac{3.6}{15} \frac{5.0}{13} \frac{4.3}{8} \frac{3.8}{5} \frac{4.3}{8} \frac{5.1}{13} \frac{4.0}{14} \frac{3.3}{25}$

+2.0 +1.3 -1.1 -0.5 0.0 -0.5 -1.2 +0.7 +1.3
 $\frac{4.5}{25} \frac{5.2}{17} \frac{7.6}{14} \frac{7.0}{10} \frac{6.5}{6} \frac{7.0}{7} \frac{7.7}{13} \frac{5.8}{15} \frac{5.2}{25}$

+2.6 +1.6 -1.1 -0.5 0.0 -0.6 -1.2 +1.1 +1.9
 $\frac{6.3}{25} \frac{7.3}{18} \frac{1.0}{15-14} \frac{9.5}{10} \frac{8.9}{9} \frac{9.5}{9} \frac{10.1}{13} \frac{7.8}{15} \frac{7.0}{25}$

+1.0 +0.2 -1.5 -0.3 0.0 -0.4 -1.3 -0.3 +0.5
 $\frac{9.5}{25} \frac{10.3}{16} \frac{12.1}{14} \frac{10.8}{6} \frac{10.5}{6} \frac{10.2}{6} \frac{11.8}{13} \frac{10.8}{14} \frac{10.0}{25}$

+0.8 -0.2 -2.0 -1.0 -0.4 0.0 -0.5 -1.3 -0.5 -0.1
 $\frac{11.4}{25} \frac{12.4}{16} \frac{14.2}{14} \frac{13.2}{10} \frac{12.6}{5} \frac{12.2}{5} \frac{12.7}{8} \frac{13.5}{13} \frac{12.7}{14} \frac{12.3}{25}$

+0.8 -0.1 -1.5 -0.8 0.0 -0.6 -1.5 -0.4 +0.1
 $\frac{2.1}{25-22} \frac{3.0}{15} \frac{4.2}{14-13} \frac{3.7}{9} \frac{2.9}{5} \frac{3.5}{8} \frac{4.4}{12-13} \frac{3.3}{14} \frac{2.8}{25}$

+1.7 +1.8 +1.2 -1.3 -0.5 0.0 -0.5 -0.9 +0.4 +0.9
 $\frac{3.3}{25} \frac{8.1}{21} \frac{3.8}{15} \frac{4.3}{15-11} \frac{5.5}{7} \frac{5.0}{5} \frac{5.5}{8} \frac{5.3}{10-12} \frac{4.6}{13} \frac{4.1}{25}$

+2.9 +2.3 -1.6 -0.8 0.0 -0.5 -1.3 +0.9 +1.9
 $\frac{3.5}{25} \frac{4.1}{16} \frac{8.0}{13} \frac{7.2}{9} \frac{6.9}{5} \frac{6.9}{6} \frac{7.7}{11} \frac{5.5}{13} \frac{4.5}{25}$

+1.1 +0.5 -1.2 -0.5 0.0 0.0 -0.7 -1.6 +0.5 +1.2
 $\frac{6.3}{25-21} \frac{7.4}{17} \frac{9.1}{14-13} \frac{8.4}{10} \frac{7.9}{7} \frac{7.9}{7} \frac{8.6}{6} \frac{9.5}{11} \frac{7.4}{13} \frac{6.7}{25}$

✓

Sta. B.S. H. I. F.S. Elev.
 10+33 1298.98 8.4 90.6

11 11.9 87.1

T.P. 2.18 1289.02 12.14 1286.84

12 6.1 82.9

13 9.7 79.3

1.4 11.3 77.7

T.P. 4.12 1280.48 12.66 1276.36

14+06 1x1' Stump & 12" V.P.
 (Req. "Pipe") 3.1 77.4

B.M. 78.37
 7.09 1273.39

14+20 4.4 76.1

15 6.0 74.5

16 11.8 68.7

T.P. 4.02 1272.77 11.73 1268.75

750 6.2 66.6

+1.2 +0.5 -1.8 -0.5 0.0 0.0 -0.4 -1.4 -2.3 +0.1 +0.2 +0.7
 $\frac{72}{25} \frac{79}{18} \frac{102}{15-14} \frac{89}{12} \frac{84}{8} \frac{84}{8} \frac{88}{5} \frac{98}{9} \frac{107}{11} \frac{83}{13} \frac{91}{21} \frac{77}{25}$

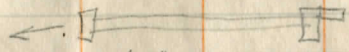
+2.4 +3.5 -0.9 -2.1 -0.7 -0.2 0.0 -0.2 -0.7 -1.5 -0.1 +1.3 +2.5
 $\frac{95}{25} \frac{84}{20} \frac{128}{72} \frac{140}{13} \frac{126}{11} \frac{121}{8} \frac{117}{8} \frac{121}{5} \frac{126}{9} \frac{134}{12} \frac{129}{13} \frac{146}{72} \frac{94}{25}$

+1.4 -1.3 -2.2 -0.7 -0.2 0.0 -0.4 -1.0 -1.7 +1.8 +1.7 +2.8 +2.9
 $\frac{47}{25-20} \frac{74}{15} \frac{83}{14} \frac{68}{10} \frac{63}{8} \frac{61}{8} \frac{65}{5} \frac{71}{8} \frac{73}{10} \frac{47}{13} \frac{14}{13} \frac{33}{21} \frac{32}{25}$

+0.1 -0.1 -1.1 -1.5 -0.8 -0.3 0.0 -0.5 -1.2 -0.2 +0.8
 $\frac{96}{25} \frac{98}{19} \frac{109}{14} \frac{112}{13} \frac{105}{10} \frac{100}{5} \frac{97}{5} \frac{102}{7} \frac{109}{11-12} \frac{99}{14} \frac{89}{25}$

-2.2 -1.9 -0.9 -0.3 0.0 -0.5 -1.1 -2.2 -1.5 -0.6
 $\frac{123}{25} \frac{132}{12-11} \frac{122}{9} \frac{115}{5} \frac{113}{5} \frac{118}{5} \frac{124}{9} \frac{135}{12} \frac{128}{13} \frac{119}{25}$

-4.9 -3.2 -2.9 12.5 2.7 0.0 -0.5 0.0 -0.9 -0.2 12.5 2.2 -0.9 -0.3
 $\frac{80}{75} \frac{63}{50} \frac{60}{25} \frac{58}{11.8} \frac{31}{11.5} \frac{36}{9} \frac{31}{9} \frac{40}{9} \frac{33}{10-12} \frac{53}{12.3} \frac{22}{13} \frac{4.0}{14} \frac{34}{25}$



← $\frac{11'-8''}{25}$ x 12 →
 Nail in the root 25" apple 40" Lt. Sta 15+45

-1.5 -1.1 -0.2 0.0 -0.4 -0.1 +0.9
 $\frac{57}{25} \frac{55}{21-13} \frac{46}{5} \frac{44}{11} \frac{43}{15} \frac{45}{25}$

+1.6 +2.1 +1.5 -1.4 -0.9 -0.3 0.0 -0.2 -0.9 -1.8 -0.4 +2.9 +3.5
 $\frac{14}{25} \frac{39}{22} \frac{45}{18} \frac{74}{14} \frac{69}{10} \frac{63}{9} \frac{60}{6} \frac{62}{6} \frac{69}{10} \frac{78}{11-12} \frac{64}{13} \frac{31}{14} \frac{2.5}{20} \frac{2.5}{25}$

+2.5 +1.7 -0.9 -0.1 +0.2 0.0 -0.3 -1.1 +4.4 +5.2
 $\frac{93}{25-20} \frac{101}{17} \frac{127}{14} \frac{119}{10} \frac{116}{3} \frac{112}{3} \frac{121}{7} \frac{129}{9} \frac{74}{16} \frac{66}{2.5} \frac{2.5}{2.5}$

+1.5 +2.0 +1.5 -1.2 -0.2 0.0 -0.2 -1.4 -2.4 +5.4 +6.0
 $\frac{47}{25} \frac{42}{21} \frac{47}{17} \frac{74}{14-13} \frac{64}{10} \frac{62}{9} \frac{64}{5} \frac{76}{9} \frac{85}{9} \frac{0.8}{19} \frac{0.8}{25}$

1272 77

17 102 62.6

+60 15.6 57.2

T.F. 1.19 1260 98 12.98 1259.79

18 7.7 53.3

T.F. 1.55 1250 29 12.24 1248.74

+75 2.7 47.6

19 3.7 46.6

19170 small brush enters ditch on Lt.

20 6.0 44.3

21 6.7 43.6

T.F. 7.48 1252 78 4.99 1245.30

+44 3'0" x 3'-4" Stone Box 8.2 44.6

(One cover stone broken)

Rt. end of box poor.

Gen. Cond. fair, Plank floor.

22 7.1 45.7

+2.9 +3.3 +2.7 -1.4 -0.4 0.0 0.0 -0.3 -2.0 -0.6 +8.7
 $\frac{23}{25} \frac{67}{22.9} \frac{75}{10} \frac{11.4}{12} \frac{10.6}{10} \frac{10.2}{7} \frac{10.2}{0} \frac{10.5}{2} \frac{12.2}{9} \frac{10.8}{10} \frac{15}{23} -2.5$

+3.8 +3.3 -0.8 -0.2 0.0 0.0 -0.2 -2.2 +0.6 +11.4
 $\frac{11.8}{25} \frac{12.3}{20} \frac{16.4}{13} \frac{15.8}{11} \frac{15.6}{6} \frac{15.6}{5} \frac{15.8}{5} \frac{17.8}{9} \frac{17.0}{11} \frac{4.2}{25} -3.0$

+3.9 +3.0 -0.7 0.0 0.0 -0.3 -2.2 +3.1 +7.7 +11.5
 $\frac{+0.3}{25} \frac{3.8}{19} \frac{4.7}{14} \frac{8.4}{11} \frac{7.7}{11} \frac{7.7}{5} \frac{8.0}{8.4} \frac{9.2}{15} \frac{4.5}{2.1} \frac{0.0}{2.1} \frac{-3.8}{25} -3.0$

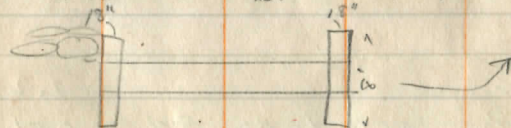
+2.4 -2.1
 $\frac{3.2}{25} \frac{-2.0}{25} \frac{-0.3}{25} \frac{+0.5}{22} \frac{+0.3}{22} \frac{+0.4}{24} \frac{-0.4}{23} \frac{-0.4}{31} \frac{-0.2}{2.9} \frac{0.0}{2.7} \frac{-0.5}{3.2} \frac{-1.2}{3.9} \frac{-2.3}{5.0} \frac{-0.9}{3.6} \frac{+0.5}{2.2} \frac{+1.9}{2.2} \frac{+2.0}{0.7}$

+0.4 -1.5 -1.3 -0.6 0.0 0.0 -0.2 -0.8 -1.4 -0.7 +1.1
 $\frac{3.3}{25} \frac{5.2}{22} \frac{5.0}{14} \frac{4.3}{12} \frac{3.7}{2} \frac{3.7}{7} \frac{3.7}{12} \frac{4.5}{14} \frac{5.1}{17} \frac{4.4}{15} \frac{2.6}{23} -2.5$

-1.3 -1.7 -2.1 -1.7 -1.2 -0.1 0.0 +0.3 -0.2 -0.3 -0.8 -0.5 0.0
 $\frac{7.3}{25} \frac{7.7}{18} \frac{8.1}{12} \frac{7.2}{13} \frac{6.1}{8} \frac{6.9}{5} \frac{6.7}{5} \frac{6.6}{5} \frac{7.1}{8} \frac{8.1}{14} \frac{7.7}{17} \frac{7.9}{21} \frac{6.5}{25} \frac{6.0}{25}$

-1.2 -0.9 -1.2 -2.1 -0.6 -0.1 0.0 +0.1 -0.4 -1.4 -1.0 -1.2
 $\frac{7.2}{25} \frac{7.6}{20} \frac{7.2}{18} \frac{8.8}{17} \frac{7.3}{10} \frac{6.8}{8} \frac{6.7}{8} \frac{6.6}{7} \frac{7.1}{13} \frac{8.1}{17} \frac{7.7}{18} \frac{7.9}{25}$

1239.8
 13.0 7.5 8.3 8.2 8.2 10.8
 Plank floor 41 Plank floor



< 12'-6" x 12'-3" >

-0.1 -0.2 0.0 -0.3 -2.6 -3.0 -2.5 -2.7
 $\frac{7.2}{25} \frac{7.3}{9} \frac{7.1}{9} \frac{7.4}{9} \frac{9.7}{14} \frac{10.1}{18} \frac{9.6}{21} \frac{9.8}{25}$

D.W.
 No ditch kept
 ext. culverts

1252.78

22+25 2 1/2 x 3' stone box

No floor
fair cond.

6.5 46.3

22+40

B.M.

5.9 46.9

32.6 1249.52

23

4.0 48.8

T.P. 12.44 1265 04

0.18 1252.60

24

8.4 56.6

T.P. 11.97 1276 45

0.56 1264.48

25

9.5 67.0

+50

4.7 71.8

26

T.P. 10.60 1286 54

2.2 74.3

0.51 1275.94

27

T.P. 9.62 1296 12

7.0 79.5

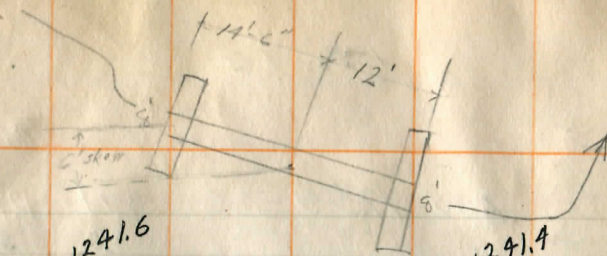
0.04 1286.50

+75

8.6 86.5

28

8.8 87.3



1241.6

1241.4

-4.7 +0.4 +0.1 0.0 -0.7 +0.2 -4.7

11.2 6.1 6.4 4.5 7.2 6.3 11.4

FL. Per 13 19.5 Per FL.

End fall

-3.1 -4.5 -4.0 -1.8 -0.2 0.0 -0.1 -1.7 -2.5 -2.0 -2.5
 90 104 92 77 61 57 60 76 84 79 84
 25 21-17 15 13 9 10.0 14 17 18 25

+2.7 +2.1 -1.2 -0.5 0.0 +0.1 -0.7 -0.3 -0.5 +1.0 +1.3
 13 17 52 4.5 4.0 3.3 4.7 4.3 4.8 3.0 2.7
 25-19 17 11 7 7 14 15 18 21 25

+7.1 +7.6 +6.4 -1.1 -0.4 +0.1 0.0 -0.7 -1.5 +6.4 +8.6
 13 0.8 2.0 9.5 8.8 8.3 8.4 9.1 9.7 2.0 1.8
 25 20 15 10 9 6 13 14 23- 25

+7.2 +5.6 +4.3 -0.6 +0.1 +0.5 0.0 -0.5 -1.4 -0.7 -0.8 +2.5
 23 39 52 101 94 90 95 100 102 102 103 70
 25 17 13 11 9 6 13 14 15 19 22-25

+0.6 -0.3 -1.3 -0.5 +0.2 0.0 -0.7 -1.4 -0.2 -0.8
 41 50 60 52 45 47 54 61 47 55
 25 74 78 71 7 11 13 15 25

+0.4 -0.5 -1.1 -0.3 0.0 -0.3 -1.8 -0.6 -1.1
 13 27 33 2.5 2.2 2.5 4.8 2.8 3.3
 25 12 10 5 2 11 13-15 25

+6.0 +3.0 -1.9 -0.3 0.0 -0.2 -1.4 -3.8 +5.7 +6.8
 10 40 39 7.3 7.0 7.2 8.4 3.2 1.3 0.2
 25-19 15 10.9 7 7 10 15 19 25

+2.7 +2.4 -1.7 -0.5 0.0 -0.1 -1.0 +1.3 +2.7 +3.2
 6.9 22 11.3 10.1 9.6 9.7 10.6 8.7 6.9 6.4
 25 14 9.8 5 9 11-12 17 21 25

+2.6 +2.8 +2.2 -0.2 -1.8 -0.7 -0.1 0.0 0.0 -1.0 -0.5 +2.6 +3.5
 6.7 10 6.6 9.0 10.6 9.5 8.9 8.8 8.9 9.3 9.3 6.2 5.8
 25 14 12 8.7 5 3 10 12-13 14 21 25

129612

29 76 91.5
 T.P. 7.35 1299 76 3.71 1292.96
 29 83 91.5

30 4.9 94.9

31 2.8 97.0

T.P. 8.93 1306 94 1.75 1298.01

32 6.6 100.3

+50 4.4 102.5

33 5.6 101.3

34 6.9 100.0

+36 15" Cor. pipe 6.1 100.8
 Pipe in good Cond.

B.M. 9.00 1310.08 5.86 1301.07
 1301.08

13

71.

00 +0.2 -0.2 -1.2 -0.4 +2.8 +3.2
~~42 42 16 44 48 58 50 18 14~~
~~2 3 5 11 13-14 15 21 25~~

L.H. 00 -0.3 -1.7 +4.1 +5.0
~~83 83 10.0 42 33~~
~~3 6 12 20~~

+1.0 +0.6 +0.9 +0.5 -0.8 -1.3 -0.3 0.0 +0.3 -0.2 -0.4 +0.4 0.0
~~39 43 40 44 57 62 52 49 46 51 53 43 4.9~~
~~25 16 18 6 2 5 3 5 12 14 15 16 2.8~~

+2.0 +1.4 +0.6 -0.7 -0.3 0.0 +0.4 0.0 -0.4 +0.2 +1.3
~~02 14 22 35 31 28 24 28 32 24 15~~
~~25 11 2 5 7 3 5 12 15 22 25~~

+4.0 2.6 -0.6 -0.2 0.0 0.0 -0.6 +0.2 +3.0 +2.8
~~26 40 72 68 66 66 72 64 36 38~~
~~25 10 2 4 6 6 13 14 21 25~~

+2.4 +1.6 -0.9 -0.4 0.0 +0.2 -0.2 -0.6 +0.1 +0.8
~~20 28 53 48 44 42 46 50 43 36~~
~~25 9 6-5 4 5 11 13-14 16 21-25~~

+3.1 +2.7 +3.0 +1.8 -0.9 -0.5 0.0 +0.2 -0.3 -0.8 -0.2 +0.6
~~25 29 26 32 45 61 56 57 53 64 53 5.0~~
~~25 18 13 10 6-5 4 5 12 14-15 16 25~~

-0.6 -0.5 0.0 +0.1 -0.3 -1.0 -0.9
~~75 74 69 68 72 79 78~~
~~25-12 9 5 15 16-18 25~~

-1.7 -2.1 -1.9 -2.3 +0.6 +0.1 0.0 +0.3 -2.6 -2.3 -4.9
~~78 82 80 84 84 60 61 61 53 8.7 84 11.0~~
~~75 50 22 9 8 5 9 11 12 25 85~~

Start cap

8' 6" x 11' 6"

Nail in S. root 24" Maple 25' Rt. 34+95.

1310 08

35

8.8 01.3

36

4.8 05.3

37

1.7 08.4

T.P. 6.75 1315 51

1.32 1308.76

38

5.4 09.9

39

3.7 11.8

40

4.4 11.1

41

5.0 10.5

42

6.5 09.0

43 a.m.

8.1 07.4

T.P. 0.31 1309 07

6.75 1308.76

44

3.1 06.0

45

4.1 05.0

46

5.7 03.9

9-29-22
Hot

Form 9
Group
spohr

14

+0.5 -0.8 -0.2 0.0 -0.2 -0.8 -0.7 +0.4 +0.4
 $\frac{8.3}{25} \frac{9.6}{21} \frac{9.0}{14} \frac{8.9}{5} \frac{9.0}{5} \frac{9.6}{15} \frac{9.5}{19} \frac{8.7}{21} \frac{8.7}{25}$

+2.6 +0.4 -2.0 -0.7 0.0 -0.2 -0.7 -1.9 +0.2 +1.6
 $\frac{2.7}{25} \frac{4.4}{14} \frac{4.8}{11-10} \frac{5.5}{8} \frac{4.8}{8} \frac{5.0}{7} \frac{5.5}{9} \frac{6.7}{11} \frac{4.6}{13} \frac{3.2}{25}$

+1.3 +0.9 -0.1 -1.5 -0.6 0.0 -0.6 -1.6 -0.3 +0.9
 $\frac{0.4}{25} \frac{0.8}{19} \frac{1.8}{13} \frac{3.2}{12-11} \frac{2.3}{8} \frac{1.7}{8} \frac{2.3}{6} \frac{3.3}{20} \frac{2.0}{11} \frac{0.8}{25}$

+1.1 -0.1 -1.0 -0.4 0.0 -0.4 -0.9 -0.1 +1.1
 $\frac{4.5}{25} \frac{5.7}{14} \frac{6.6}{12} \frac{6.0}{8} \frac{5.4}{8} \frac{6.0}{6} \frac{6.5}{9} \frac{5.7}{10} \frac{4.5}{25}$

+0.1 -0.3 -1.2 -0.7 -0.1 0.0 -0.4 -1.0 -0.2 +0.4
 $\frac{3.6}{25} \frac{4.8}{20} \frac{4.9}{18-14} \frac{4.1}{13} \frac{3.8}{10} \frac{3.7}{10} \frac{4.1}{6} \frac{4.7}{9} \frac{3.9}{10} \frac{3.3}{25}$

-0.1 -0.5 -0.9 -0.3 0.0 0.0 -0.3 -0.8 -0.4 +0.3
 $\frac{4.5}{25} \frac{4.7}{21} \frac{5.3}{14} \frac{4.7}{12} \frac{4.4}{7} \frac{4.4}{2} \frac{4.7}{6} \frac{5.2}{9} \frac{4.8}{11} \frac{4.1}{25}$

0.0 -0.1 -0.7 -1.3 -0.6 0.0 -0.6 -1.4 -0.6 -0.1
 $\frac{5.0}{25} \frac{5.1}{19} \frac{5.7}{14} \frac{6.3}{12} \frac{5.6}{8} \frac{5.0}{8} \frac{5.6}{6} \frac{6.4}{9-10} \frac{5.6}{11} \frac{5.1}{25}$

+0.5 -0.1 -1.1 -0.7 -0.3 0.0 -0.5 -1.1 -0.3 -0.1 -0.2
 $\frac{6.0}{25} \frac{6.5}{15} \frac{7.6}{14-13} \frac{7.2}{12} \frac{6.8}{8} \frac{6.5}{8} \frac{7.0}{6} \frac{7.6}{20} \frac{6.8}{11} \frac{6.6}{19} \frac{6.7}{25}$

11.0 +0.8 0.0 -1.0 -0.4 0.0 -0.5 -0.9 +0.4 +0.8 +1.1
 $\frac{7.1}{25} \frac{7.3}{22} \frac{8.1}{15} \frac{8.1}{14-13} \frac{8.5}{10} \frac{8.1}{10} \frac{8.5}{6} \frac{9.0}{8-9} \frac{7.7}{11} \frac{7.3}{13} \frac{7.0}{25}$

Hail in trail

+1.4 +0.8 -0.3 -1.0 -0.4 +0.1 0.0 -0.5 -0.9 -0.4 +0.1
 $\frac{1.7}{25} \frac{2.3}{20} \frac{3.4}{15} \frac{4.1}{14-13} \frac{3.5}{11} \frac{3.0}{2} \frac{3.1}{2} \frac{3.6}{6} \frac{4.0}{7.8} \frac{3.5}{9} \frac{3.0}{15-25}$

+0.7 -0.7 -1.1 -0.7 -0.2 0.0 -1.1 -0.6 -0.5
 $\frac{3.4}{25} \frac{4.8}{15} \frac{5.2}{14} \frac{4.8}{11} \frac{4.3}{7} \frac{4.1}{7} \frac{5.2}{9} \frac{4.7}{10} \frac{4.6}{25}$

+0.6 -0.5 -0.9 -0.4 0.0 -0.7 -0.5 -0.6
 $\frac{4.6}{25} \frac{3.7}{15} \frac{4.1}{14} \frac{5.6}{9} \frac{5.2}{7} \frac{5.3}{9} \frac{5.7}{9} \frac{5.0}{15}$

1
1309 07

47

5.0

03.2

48

6.6

02.5

49

7.0

02.1

J.M.

2.65

1306.85

4.87

1304.20

50

4.7

02.2

51

4.5

02.4

52

4.3

02.6

53

4.5

02.4

54

4.4

02.5

55

4.0

02.9

56

2.8

04.1

T.P.

4.90

1309 29

2.46

1304.35

15

-0.4 -0.5 -0.7 -0.4 0.0 0.0 -0.3 -0.7 -0.5 -1.1
 $\frac{6.3}{25} \frac{6.4}{14} \frac{6.5}{12} \frac{6.3}{9} \frac{5.7}{3} \frac{5.7}{6} \frac{6.2}{9} \frac{5.6}{9} \frac{6.7}{10} \frac{7.0}{25}$

-0.7 -0.3 -0.5 -0.1 0.0 -0.7 -0.4 -0.7
 $\frac{7.0}{25} \frac{5.9}{14} \frac{7.1}{13} \frac{6.7}{6} \frac{6.6}{9} \frac{7.3}{9} \frac{7.0}{10} \frac{7.3}{25}$

+0.6 -0.4 -0.7 -0.3 +0.1 0.0 -0.5 0.0 +0.5
 $\frac{6.4}{25} \frac{7.4}{15} \frac{7.3}{13} \frac{7.3}{11} \frac{6.9}{7} \frac{7.0}{7} \frac{7.8}{11} \frac{7.0}{11} \frac{6.6}{25}$

Spike in N. side 12" Maple 'Lt. Sta.

-0.2 -0.3 -0.9 -0.2 0.0 -0.4 -0.7 -0.3 -0.2
 $\frac{4.7}{25} \frac{5.0}{14} \frac{5.5}{12} \frac{4.7}{8} \frac{4.7}{9} \frac{5.1}{5} \frac{5.4}{10-11} \frac{5.0}{12} \frac{4.7}{25}$

-0.6 -0.4 -0.9 -0.5 0.0 0.0 -0.4 -1.0 -0.5 -0.3
 $\frac{5.1}{25} \frac{4.7}{14} \frac{5.4}{13} \frac{5.0}{9} \frac{4.5}{2} \frac{4.7}{9} \frac{5.3}{11-12} \frac{5.0}{13} \frac{4.8}{25}$

0.0 -0.7 -1.1 -0.6 0.0 -0.6 -0.2 -0.8 -0.2
 $\frac{4.3}{25} \frac{5.0}{14} \frac{5.4}{12} \frac{4.7}{8} \frac{4.3}{7} \frac{4.7}{10} \frac{5.5}{12-13} \frac{5.1}{14} \frac{4.5}{25}$

-0.2 -0.4 -1.1 -0.7 0.0 +0.1 -0.5 -1.0 -0.6 -0.8
 $\frac{4.7}{25} \frac{4.7}{13} \frac{5.6}{11} \frac{5.2}{9} \frac{4.5}{4.5} \frac{4.4}{2} \frac{5.0}{12} \frac{5.5}{13} \frac{5.1}{15} \frac{5.3}{25}$

-0.4 -0.9 0.0 +0.1 -0.3 -1.0 -0.6 -0.5
 $\frac{4.8}{25} \frac{5.3}{12} \frac{5.3}{10} \frac{4.4}{4.4} \frac{4.3}{7} \frac{4.7}{13} \frac{5.4}{15} \frac{5.0}{16} \frac{4.7}{25}$

+0.3 -0.2 -1.0 0.0 +0.1 -0.2 -0.6 -0.1 +0.2
 $\frac{3.7}{25} \frac{4.2}{11} \frac{5.0}{12} \frac{4.0}{4.0} \frac{4.7}{7} \frac{4.2}{13} \frac{4.6}{16} \frac{4.1}{17} \frac{3.8}{25}$

+0.7 0.0 -1.0 0.0 -0.2 -0.8 +0.1 +0.9
 $\frac{2.1}{25} \frac{2.1}{12} \frac{3.8}{10} \frac{2.5}{2.5} \frac{3.8}{13} \frac{3.6}{16} \frac{2.7}{18} \frac{1.9}{25}$

1309³29

57 4.0 05.3
 +90 24'-12 Cor Pipe (end) 37 05.6
 (Repd 12' sq. with E)

58 3.6 05.7

59 3.8 05.5
 B.M. 492 1304.37

T.P. 685 1313.00 314 1306.15

60 6.4 06.6

61 4.1 1308.9

+50 5.4 07.6

62 7.0 06.0

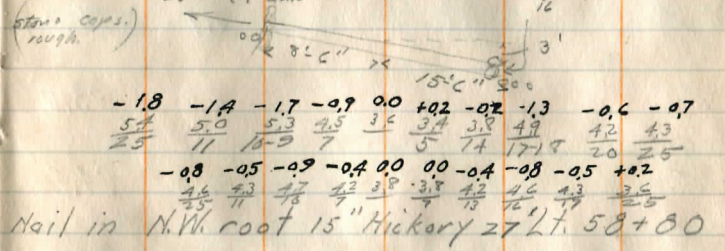
63 8.3 04.7

64 9.8 03.2

65 13.0 1300.0

T.P. 0.82 1301.12 12.70 1300.30

-0.6 +0.2 0.0 -0.7 0.0 +0.2 -0.2 -0.4 +0.2 +1.1
 $\frac{16}{25} \frac{38}{12} \frac{4.0}{70} \frac{4.7}{9} \frac{4.2}{5} \frac{4.2}{14} \frac{4.4}{16} \frac{3.8}{17} \frac{2.9}{25}$
 1303.3
 -3.6 -2.1 -2.3 +0.3 -0.2 0.0 +0.2 +0.7 -1.6 -1.5 -0.3 0.0
 $\frac{23}{50} \frac{5.8}{25} \frac{0.0}{21} \frac{3.4}{25} \frac{3.7}{5} \frac{3.7}{12} \frac{3.5}{12} \frac{3.0}{12} \frac{1304.0}{16} \frac{5.3}{16} \frac{5.2}{19} \frac{4.0}{20} \frac{3.7}{23}$



-1.8 -1.4 -1.7 -0.9 0.0 +0.2 -0.2 -1.3 -0.6 -0.7
 $\frac{5.4}{25} \frac{5.0}{11} \frac{5.3}{15} \frac{4.3}{7} \frac{3.5}{5} \frac{3.4}{5} \frac{3.8}{7.4} \frac{4.8}{17.9} \frac{4.2}{20} \frac{4.3}{25}$

-0.8 -0.5 -0.9 -0.4 0.0 0.0 -0.4 -0.8 -0.5 +0.2
 $\frac{4.6}{25} \frac{5.3}{11} \frac{4.7}{18} \frac{4.2}{7} \frac{3.8}{5} \frac{3.8}{12} \frac{4.6}{16} \frac{4.3}{17} \frac{3.6}{25}$
 Nail in N.W. root 15" Hickory 27 Lt. 58+00

-0.2 -0.7 -0.5 0.0 -0.7 -1.1 -0.2 +0.9
 $\frac{6.6}{25} \frac{7.1}{9} \frac{6.8}{9} \frac{4.4}{4} \frac{7.2}{12} \frac{7.5}{13} \frac{1.4}{19} \frac{6.6}{15} \frac{5.5}{25}$

+1.2 +0.3 -0.6 -0.4 +0.1 0.0 -0.6 +0.2 +1.1
 $\frac{2.9}{25} \frac{3.8}{14} \frac{4.7}{13} \frac{4.5}{10} \frac{4.0}{7} \frac{1.1}{7} \frac{4.7}{11} \frac{3.2}{13} \frac{3.8}{18} \frac{2.5}{25}$

+1.6 +1.0 +0.1 -0.9 -0.5 +0.1 0.0 -0.4 -0.5 +2.7 +2.9
 $\frac{0.8}{25} \frac{4.4}{17} \frac{5.3}{14} \frac{6.3}{13} \frac{5.9}{9} \frac{5.3}{2} \frac{5.4}{4} \frac{5.3}{9} \frac{5.7}{11} \frac{2.1}{13} \frac{2.5}{25}$

+1.6 0.0 -0.7 +0.2 0.0 -0.4 -0.8 +1.8 +2.0
 $\frac{5.4}{25} \frac{7.0}{14} \frac{7.7}{13} \frac{6.3}{5} \frac{2.0}{2} \frac{7.4}{9} \frac{7.8}{11} \frac{5.5}{12} \frac{5.0}{25}$

-0.4 -0.1 -0.8 -0.1 0.0 -0.2 -0.8 -0.2 -1.2 -1.6
 $\frac{8.7}{25} \frac{8.4}{13} \frac{8.1}{12} \frac{8.4}{3} \frac{8.3}{7} \frac{8.5}{11} \frac{8.5}{12} \frac{3.5}{22} \frac{9.9}{25}$

+1.5 +0.6 -0.6 -1.3 -0.6 0.0 -0.7 -1.3 -0.8 -0.1 +0.9
 $\frac{8.3}{25} \frac{9.0}{12} \frac{10.4}{15} \frac{11.1}{12} \frac{10.4}{8} \frac{9.3}{9} \frac{10.5}{11} \frac{11.1}{12} \frac{10.6}{13} \frac{9.7}{18} \frac{9.5}{25}$

0.0 -0.7 -1.6 -0.9 0.0 -0.4 -1.4 +1.7 +2.2
 $\frac{13.0}{25} \frac{13.7}{13} \frac{14.6}{12} \frac{13.9}{9} \frac{13.0}{13} \frac{13.4}{9} \frac{14.4}{11} \frac{11.3}{17} \frac{10.8}{25}$

✓

130112

66 3.8 97.3

67 5.1 96.0

68 6.0 95.1

69 6.9 94.2

70 7.4 93.7

71 9.8 91.3

72 3.3 89.8

+53 old filled stant (bar)??
do nothing - H.G. & not req'd. 3.5 89.6

73 4.4 88.7

+82 12" C.I. P. -18'
G.V.P.
(Remove, Reel 15") 5.0 88.1

74 5.2 87.9

+40 old filled up pipe N.G.
No work omit. 4.9 88.2

-0.2 +0.1 -0.9 -0.2 0.0 -0.2 -0.5 -1.0 -0.4 +0.9 +2.1 +2.3
 $\frac{4.0}{25-18} \frac{3.7}{13} \frac{4.7}{12-10} \frac{4.0}{5} \frac{3.9}{5} \frac{4.0}{5} \frac{4.3}{8} \frac{4.8}{9-10} \frac{4.3}{11-13} \frac{2.9}{14} \frac{1.7}{18} \frac{1.5}{2.5}$

0.0 -0.3 -0.9 -0.1 0.0 -0.5 -1.2 -0.3 +0.6 +0.7
 $\frac{5.1}{25} \frac{5.4}{13} \frac{6.0}{12} \frac{5.2}{9} \frac{5.1}{9} \frac{5.5}{7} \frac{6.3}{10-12} \frac{5.4}{13} \frac{4.5}{17} \frac{4.4}{25}$

-0.8 -0.6 -1.1 -0.7 -0.2 0.0 -0.3 -1.6 -0.5 -0.6
 $\frac{5.8}{25} \frac{6.6}{13} \frac{7.1}{12} \frac{6.7}{9} \frac{6.2}{5} \frac{6.0}{5} \frac{6.3}{6} \frac{7.6}{11-12} \frac{6.5}{13} \frac{6.6}{25}$

-0.1 -0.6 -1.0 -0.7 0.0 -0.2 -0.8 -1.3 -1.4 -0.9
 $\frac{7.0}{25} \frac{7.5}{21-13} \frac{7.9}{12-10} \frac{7.6}{9} \frac{6.9}{9} \frac{7.1}{4} \frac{7.7}{9} \frac{8.2}{12} \frac{7.3}{13} \frac{7.8}{25}$

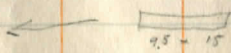
+1.7 +1.4 +0.1 -0.8 -1.7 -0.8 0.0 -0.2 -0.9 -1.6 -0.6 +1.0
 $\frac{5.7}{25} \frac{6.0}{22} \frac{7.3}{12} \frac{8.2}{13} \frac{9.1}{12-11} \frac{8.2}{8} \frac{7.4}{8} \frac{7.6}{6} \frac{8.3}{10} \frac{9.0}{12} \frac{8.0}{14} \frac{8.4}{25}$

+3.3 +2.8 +0.7 -1.0 -0.3 0.0 -0.4 -1.4 +0.8 +0.9
 $\frac{6.5}{25} \frac{7.0}{16} \frac{9.1}{11} \frac{10.5}{10-9} \frac{10.1}{7} \frac{9.8}{7} \frac{10.2}{8} \frac{11.2}{11-12} \frac{9.0}{15} \frac{8.9}{25}$

-0.3 -0.5 0.0 -0.3 -0.8 -0.3 -0.4
 $\frac{3.6}{25-12} \frac{3.3}{11} \frac{3.3}{8} \frac{3.6}{8} \frac{4.1}{12-13} \frac{3.6}{14} \frac{3.1}{25}$

-1.2 -0.8 -0.9 0.0 -0.2 -0.9 -0.6 -0.4
 $\frac{5.6}{25} \frac{5.2}{23-13} \frac{5.3}{11} \frac{4.1}{16} \frac{4.6}{14} \frac{5.3}{14} \frac{5.0}{15} \frac{4.8}{25}$

12.857 12.868
 -4.5 -2.9 -2.4 -1.7 -1.7 -0.5 0.0 +0.3 -1.3 -0.9 -0.2 +0.8
 $\frac{9.5}{175} \frac{7.9}{125} \frac{7.4}{75} \frac{6.7}{25} \frac{6.7}{14} \frac{5.5}{9.5} \frac{5.0}{9} \frac{4.7}{15} \frac{6.3}{16.1} \frac{5.9}{17} \frac{5.2}{18} \frac{4.3}{25}$

(2nd outlet reel) ←  9.5 - 15

-1.0 -0.5 -0.7 -0.3 0.0 +0.2 0.0 -0.2 0.0 -0.8 -0.2 +0.2
 $\frac{6.2}{25} \frac{5.7}{11} \frac{5.4}{10} \frac{5.5}{9} \frac{5.2}{9} \frac{5.0}{4} \frac{5.2}{12} \frac{5.4}{14} \frac{5.7}{15} \frac{6.0}{16} \frac{5.4}{17} \frac{5.0}{25}$

1293 12

75 5.1 88.0

76 4.9 88.2

77 7.5 85.6
 J.M. 8.75 1284.37
 T.P. 5.28 1290 26 8.14 1284.98
 75+75 1.7 88.6

77+ 6 5.6 84.7
 6.7 83.6
 8.2 82.1
 6.3 84.0
 7.2 83.1
 78 6.7 83.6

79 Moon 9.4 80.9
 T.P. 1.72 1280 76 11.22 1279.04
 80 2.1 78.7
 3.2 77.6
 4.2 76.6
 4.4 76.4
 4.6 76.2

-0.5 -0.3 -0.8 -0.6 0.0 -0.1 -0.6 0.0 +1.0
 $\frac{5.6}{25} \frac{5.4}{12} \frac{5.7}{11} \frac{5.7}{8} \frac{5.1}{7} \frac{5.2}{7} \frac{5.7}{11} \frac{5.1}{12} \frac{4.1}{25}$

+0.6 +1.0 +0.5 -0.3 -0.6 0.0 -0.3 +0.6 +1.4 +2.2
 $\frac{4.3}{25} \frac{3.9}{20} \frac{4.4}{14} \frac{5.8}{12} \frac{3.5}{9} \frac{4.9}{1} \frac{6.2}{7} \frac{4.3}{15} \frac{3.5}{12} \frac{2.7}{25}$

+1.5 +0.8 -0.3 -0.1 0.0 -0.2 +1.2 +2.3
 $\frac{6.0}{25} \frac{6.7}{22} \frac{7.2}{13} \frac{7.6}{12} \frac{7.6}{6} \frac{7.5}{15} \frac{7.7}{8} \frac{6.3}{11} \frac{5.2}{12} \frac{5.2}{25}$

+1.2 +1.0 -0.8 -0.5 0.0 0.0 +0.2 +1.7 +2.7
 $\frac{0.5}{25} \frac{0.7}{13} \frac{2.5}{11} \frac{2.7}{8} \frac{1.7}{1} \frac{1.7}{8} \frac{1.5}{10} \frac{-0.2}{12} \frac{-1.0}{25}$

Nail in NW root 40" Elm Lt. W. side Ctr Rd.

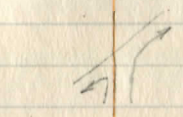
E Ctr. Rd.
 100' Rt.
 200' Rt.
 100' Lt.
 200' Lt.

12.1 +1.2 +0.2 -0.5 0.0 0.0 +0.7 +0.4
 $\frac{4.6}{25} \frac{3.8}{21} \frac{5.5}{14} \frac{7.2}{13} \frac{6.7}{5} \frac{6.7}{18} \frac{6.0}{18} \frac{6.3}{25}$ in Rd.

+1.2 +1.0 -0.1 -0.8 0.0 0.0 -0.5 -0.8 +0.2 +2.4 +2.5
 $\frac{3.3}{25} \frac{3.4}{21} \frac{3.5}{17} \frac{10.2}{12} \frac{9.4}{5} \frac{4.1}{1} \frac{9.2}{5} \frac{10.5}{7} \frac{9.2}{8} \frac{7.0}{20} \frac{6.0}{25}$

+2.0 +1.0 -0.5 -0.9 -0.5 +0.5 0.0 -0.6 -1.2 +0.2 +1.1
 $\frac{0.1}{25} \frac{1.1}{21} \frac{2.6}{19} \frac{3.0}{17} \frac{2.6}{15} \frac{1.6}{6} \frac{2.1}{1} \frac{2.7}{5} \frac{3.3}{2.7} \frac{1.9}{8} \frac{1.0}{25}$

E Rd to Lt.
 " " Lt.
 50' " "
 100' " "
 150' " "



128076

81				5.4	75.4
82				8.0	72.8
83				9.5	71.3
T.F.	3.85	1275	30	9.31	1271.45
84				4.7	70.6
+09	22 ft.	16" Cor pipe		4.2	71.1
		new, good			
85					
86				2.2	73.1
T.F.	8.64	1282	2.1	1.73	1273.57
87				6.5	75.7
88				4.4	77.8
+25				4.0	78.2
89				7.1	75.1

+1.3	-0.4	+0.3	0.0	-0.4	+0.7	+1.3	+1.6		
4.1	5.8	5.1	5.4	5.8	4.7	4.1	3.8		
2.5	13-16	4		5-8	9	17	25		
+1.5	+0.8	-0.8	-0.2	+0.6	0.0	-0.8	+0.6	+1.3	
6.5	7.2	8.8	8.2	7.4	8.0	8.8	7.4	6.7	
2.5	17	15-14	12	2		8	9	17-25	
+0.6	0.0	-0.7	-0.4	+0.1	0.0	-0.8	-0.1	+0.2	
8.2	9.5	10.2		9.2	9.4	9.5	10.3	9.6	
2.5	15	14-12	7	3	2		8-10	11	
								2.5	
-1.3	-2.0	-0.4	0.0	+0.2	-0.1	-1.8	-1.4	-1.7	-1.5
6.0	6.7	5.1	4.7	4.5	4.8	5.5	6.1	5.4	6.2
2.5	12	11-9	7	2	10	12	13	18	2.5
-4.6	-4.0	-3.8	-4.1	-0.9	0.0	0.0	-3.2	-3.2	-2.4
8.8	8.2	8.0	8.3	5.1	4.2	4.2	7.4	7.4	6.6
6.5	4.0	1.8	FL	10.0		11	FL	12	1.8
									3 1/2 - new - 8 1/2
									10' 1/2" x 11'-2"
-0.6	-0.3	-0.9	-0.5	0.0	-0.1	-0.4	+1.4	+2.0	
4.2	1.6	5.2	4.8	4.3	4.4	5.7	2.8	2.3	
2.5	1.3	12-11	10		8	12	15	2.5	
0.0	+0.4	+0.2	-1.5	-1.0	0.0	-0.3	-0.6	+0.4	+1.9
2.2	1.7	2.0	3.7	3.2	2.2	3.5	2.3	1.5	0.3
2.3	1.5	1.5	1.3	1.1		8	7-11	1.5	2.5
+0.7	+0.6	-0.4	-1.3	-0.7	0.0	-0.2	-1.0	+0.4	+2.0
5.8	5.9	6.7	7.8	7.2	9.5	6.7	7.3	6.1	4.5
2.5	1.5	1.3	12-11	9		8	11-12	1.5	2.5
+0.3	+0.6	+0.2	-1.1	-0.6	0.0	+0.2	-0.4	-0.8	+0.2
4.1	3.9	4.2	5.5	5.0	4.4	4.2	4.8	5.2	4.2
2.5	2.1	1.2	11-10	8		2	4	12-13	1.4
									2.5
+0.5	+0.3	-1.2	-0.8	0.0	0.0	-0.6	-1.1	-0.3	+0.7
3.5	3.7	5.2	4.8	4.0	4.0	4.6	5.1	4.3	3.3
2.5	1.3	11-10	9		2	1.5	11-12	1.3	2.5
+1.4	-0.4	0.0	+0.2	-0.6	+1.2	-0.3	-0.3	+0.7	
5.7	7.5	1.1	1.6	7.3	8.3	7.4	6.4	6.4	
2.5	1.2	1.0	3	11	13-14	1.5	2.5	2.5	

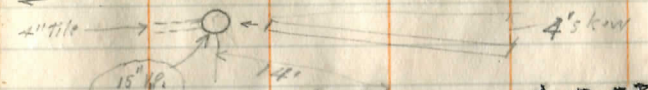
128221

90			9.2	73.0
91			10.2	72.0
T.P.	41.4	1275	67	10.68 1271.53
91+82	24' 10 5/8" 12" Iron pipe (Reqd Max 12")		4.3	71.4
92			4.5	71.2
93			4.8	70.9
94			5.0	70.7
95			5.9	69.8
96			7.7	68.1
B.M.			5.55	1270.12
T.P.	3.94	1269	65	9.96 1265.71
97			4.4	65.3
98			7.2	62.5

+0.4	+0.1	-1.3	-0.7	0.0	-0.6	-0.2	+0.2
8.8	9.1	1.95	9.7	9.2	9.8	9.4	9.0
2.5	12	10	8		10-13	14	2.5

-1.2	-0.7	-1.3	-1.0	0.0	0.0	-0.5	-0.3	+0.1
11.4	10.2	11.5	11.2	10.2	10.2	10.7	10.5	10.1
2.5	12	11	9		2	12	14	2.5

-2.0	12.69.2	-2.2	-0.5	0.0	0.0	-1.7	-1.7	-0.9
6.35		6.5	4.8	4.3	4.3	6.0	6.0	5.2
14.7		14.10	14	14	14	14	14	17



-1.2	-0.8	-1.2	-0.0	0.0	-0.2	-0.7	-1.0	-0.7	-0.0
5.7	5.3	5.7	5.4	4.5	4.7	4.9	5.5	5.2	4.5
2.5	13	12	11	13	9	12	13	14	2.5

-0.2	-1.1	-0.9	-0.4	0.0	-0.5	-0.8	-0.3	+0.4
5.0	5.9	5.7	5.2	4.3	5.3	5.6	5.1	4.4
15	11	10	10	10	10	12	13	2.5

-1.0	-0.4	-0.8	-1.2	-0.8	0.0	-0.4	-0.8	-0.2	+0.2
6.8	5.4	5.8	6.2	5.8	5.0	5.4	5.9	5.2	4.8
2.5	2.0	17	13	12	9	7	10	12	2.5

-0.6	-0.3	-1.1	-0.6	-0.1	0.0	-0.4	+0.3	+1.5
6.5	6.2	7.0	6.5	6.0	5.2	6.3	5.6	4.4
2.5	17	13	11	5		11		2.5

-0.1	0.0	-0.2	0.0	-0.3	+0.2	+0.8	+1.5
7.8	7.7	7.9	7.7	8.0	7.5	6.9	6.2
2.5	18	9		12	10	12	2.5

Nail in S. root 4' Chestnut Rt.

+0.6	+0.4	-0.4	+0.1	0.0	0.0	-0.4	+0.2	+1.5
3.8	4.0	4.3	4.3	4.4	4.4	4.8	4.2	2.9
2.5	10	10	4	4	6	8-9	10-14	2.5

-0.2	-0.3	-0.8	-0.3	0.0	+0.1	-0.3	+1.1	+1.5	+1.6
7.4	7.5	7.0	7.5	7.2	7.1	7.5	6.1	5.7	5.6
2.5	13	12-10	11	11	5	11	11	16	2.5

1269 65

99 10.2 59.5

T.P. 2.20 1260 26 11.59 1258.06
100 3.0 57.3

+50 4.3 56.0

100+2470 +53 9" 7 1/2 m. H. ditch

101 7.1 53.2

+30 9.8 50.5

T.P. 1.46 1249 9.9 11.73 1248.53

102 9.8 40.2

T.P. 1.12 1238 6.6 12.45 1237.54

103 9.8 28.9

T.P. 6.20 1227 12 12.74 1225.92

104 5.1 22.0

1224.31

J.M. 2.82 1224.30

105 10.1 17.0

T.P. 3.67 1217 8.6 12.93 1214.19

106 4.3 13.6

quit
T.P. 2.08 1214 8.9 5.05 1212.81

107 4.1 10.8

108 6.2 08.7

prepared

108+90 new location for 12" hillside 7.4 07.5

9-30-22
Hot
Fair

Hanna
Group
open

21

-0.6 +0.2 -0.1 -0.7 -0.3 +0.1 0.0 -0.7 -1.0 -1.4 -0.6 +0.3 +2.0
108 100 103 107 105 101 102 10.9 11.2 11.4 10.8 20 8.2
25 13 12 11-10 9 3 10 7 10 11 12 21 25
rock

+1.2 +0.8 -0.9 -0.4 +0.2 0.0 -0.7 -1.1 -0.4 -0.5 +1.4 +1.7
1.8 2.2 3.9 3.4 2.8 3.0 3.7 4.1 3.4 3.5 1.6 1.3
25 15 13-12 10 2 3 9 11 12 19 23 25

+1.2 +0.5 0.0 -0.3 0.0 -0.7 -1.3 -0.3 +1.2 +1.6
3.1 3.8 4.3 4.6 4.3 5.0 5.6 4.6 3.1 2.7
25 7 14 10 9 11 12-17 21 25

+2.1 +2.0 -0.6 -0.2 0.0 +0.1 0.0 -0.3 -1.5 -0.5 +1.0 +2.0
5.0 5.1 7.7 7.3 7.1 7.2 7.1 7.4 8.5 7.5 6.1 5.1
25 22 17 16 13 3 5 10-11 12 18 25
rock

+2.3 +2.1 -0.7 0.0 0.0 -1.0 -2.0 +1.6 +2.6
2.5 2.7 10.5 9.3 9.9 10.7 4.3 8.2 7.2
25 20 18 12 rock 10-11 17 25

+1.6 +1.3 -1.4 -0.9 -0.6 0.0 -1.3 -2.7 -0.9 -0.4 +1.1
8.2 8.5 11.2 10.7 10.4 9.2 11.1 10.7 10.7 10.2 9.7
25 19 15-14 13 4 7 8-10 11 17 25
rock

+1.2 +0.9 -2.6 -1.4 -0.7 0.0 -0.4 -1.3 -1.9 -1.1 +0.1 +0.8 +1.3
8.5 8.3 12.4 11.2 10.8 9.8 10.2 11.1 11.7 10.9 9.7 9.0 8.5
25 14 12 10 7 3-6 10 11 12 15 18 25
rock

+1.4 +1.0 +0.6 -1.8 -1.1 -0.4 0.0 0.0 -0.4 -2.3 +0.4 +1.8
3.7 4.1 4.5 6.9 6.2 5.5 5.1 5.1 5.5 7.4 9.7 3.3
25 7 7 7 8-4 5 10 13-14 16 19-25

Nail in S.W. root 15" Apple 35' Rt. Sta 104

+0.7 +0.8 +0.1 -1.4 -0.9 -0.3 0.0 +0.1 -0.5 -1.8 -0.9 +0.5 +1.6
9.2 9.3 10.0 11.7 11.0 10.4 10.1 10.0 10.6 11.4 11.0 9.6 8.5
25 19 11 10.9 8 4 4 10 12-13 14 18 25

-0.1 -0.5 -1.6 -1.8 -0.5 0.0 -0.3 -1.7 -0.8 0.0
4.4 4.3 5.9 4.3 4.6 6.0 5.1 4.3
25 11 10.9 6 5 13-15 16 25

spike into

-0.3 -0.6 -0.8 0.0 +0.1 -0.5 -0.9 -0.4
4.3 4.7 4.1 4.1 4.5 5.0 4.5
25 11 10.9 4 5 7.2 13-14 15-25

-0.5 -0.9 -0.5 0.0 0.0 -0.5 -1.1
6.7 7.1 6.7 6.2 6.1 7.3
25 12 11-4 14 20 25

-1.0 -0.3 -0.8 -0.2 0.0 +0.1 -0.3 -0.9 -4.4 -5.5
8.4 7.7 9.3 7.6 7.1 7.7 8.3 11.8 12.9
20 12 10 6 14 25 7.5 100

1214⁹ 89

109 7.5 07.4

110 8.6 06.3

111 9.7 05.2

T.P. 5.21 1209⁶ 57 10.53 1204.36

112 5.5 04.1

113 7.3 02.3

114 9.4 00.2

B.M. 8.39 1201.18

115 11.5 98.1

T.P. 1.84 1199⁶ 58 11.23 1197.74

116 3.1 96.5

+60 3.5 96.1

117 6.0 93.6

+50 8.3 91.3

✓

-1.2 -1.0 -0.4 -0.9 -0.4 0.0 +0.2 -0.3 -0.1 -0.8
 $\frac{87}{25} \frac{65}{12} \frac{77}{9} \frac{84}{8} \frac{72}{5} \frac{75}{5} \frac{73}{5} \frac{78}{14} \frac{76}{17} \frac{83}{25}$

-1.0 -0.9 -1.3 -0.3 0.0 +0.2 -0.7 -0.4 -1.4
 $\frac{86}{25} \frac{95}{10} \frac{97}{9} \frac{89}{5} \frac{86}{5} \frac{84}{5} \frac{93}{13} \frac{90}{15} \frac{10.0}{25}$

+0.3 -0.3 -1.3 -0.6 0.0 +0.4 -0.5 -1.0 -0.3 +0.2
 $\frac{84}{25} \frac{100}{11} \frac{110}{10} \frac{103}{6} \frac{97}{4} \frac{83}{4} \frac{102}{13} \frac{107}{14} \frac{100}{15} \frac{95}{25}$

+1.4 +0.8 -0.1 -1.6 -1.1 -0.3 0.0 +0.1 -0.8 -1.4 +0.1 +0.2
 $\frac{41}{25} \frac{47}{17} \frac{56}{11} \frac{71}{10} \frac{66}{9} \frac{58}{4} \frac{55}{5} \frac{54}{5} \frac{63}{12} \frac{63}{14} \frac{54}{15} \frac{51}{17} \frac{51}{25}$

+2.5 +2.0 +0.9 -1.7 -0.4 0.0 +0.1 -0.7 -1.2 -0.3 +0.9 +1.0
 $\frac{48}{25} \frac{53}{15} \frac{64}{12} \frac{20}{9} \frac{22}{8} \frac{73}{5} \frac{23}{4} \frac{80}{12} \frac{85}{13} \frac{76}{14} \frac{64}{15} \frac{63}{17} \frac{63}{25}$

+1.2 +0.2 -1.7 -0.4 0.0 +0.1 -0.2 -0.9 +0.3 -0.3
 $\frac{52}{25} \frac{92}{12} \frac{111}{9} \frac{98}{6} \frac{94}{6} \frac{93}{4} \frac{96}{12} \frac{103}{13} \frac{91}{15} \frac{97}{25}$

spike in 3 root of Chestnut 17' Rk. Sta. 114 + 90

+2.8 +1.1 -1.1 -0.4 -0.1 0.0 -0.1 -0.9 -1.3 +2.1 +1.5
 $\frac{87}{25} \frac{104}{15} \frac{126}{12} \frac{119}{10} \frac{116}{7} \frac{115}{3} \frac{116}{2} \frac{124}{8} \frac{123}{10} \frac{94}{11} \frac{102}{15} \frac{102}{25}$

May need 20'-12" in ditch in Rk to save chestnut tree.

+0.8 -0.3 -0.8 0.0 0.0 -0.7 +0.1 +0.4 0.0
 $\frac{23}{25} \frac{34}{14} \frac{39}{10} \frac{31}{2} \frac{31}{2} \frac{38}{10} \frac{30}{11} \frac{27}{12} \frac{31}{21} \frac{31}{25}$

+0.9 +0.3 -0.9 -1.4 -0.7 0.0 -0.2 -0.9 -1.8 -0.6 -1.2 -1.8
 $\frac{26}{25} \frac{33}{17} \frac{44}{12} \frac{49}{11} \frac{42}{7} \frac{35}{7} \frac{37}{4} \frac{44}{9} \frac{53}{11} \frac{41}{12} \frac{47}{12} \frac{53}{25}$

+2.6 +2.0 +0.1 -0.3 -2.0 -1.0 -0.4 0.0 -0.8 -1.4 -2.5 -0.1 +1.0 +2.2 -0.2
 $\frac{34}{25} \frac{40}{18} \frac{59}{15} \frac{63}{12} \frac{80}{11} \frac{70}{7} \frac{64}{5} \frac{60}{5} \frac{68}{7} \frac{74}{9} \frac{85}{10} \frac{61}{12} \frac{50}{14} \frac{58}{20} \frac{62}{25}$

+4.6 +4.4 0.0 -1.4 -0.6 0.0 -0.1 -1.0 -1.3 +2.7 +2.6 +2.2
 $\frac{37}{25} \frac{37}{18} \frac{57}{12} \frac{47}{11} \frac{29}{7} \frac{73}{7} \frac{34}{2} \frac{93}{9} \frac{96}{13} \frac{76}{11} \frac{57}{14} \frac{61}{25}$

1199 58

118

96 90.0

+60

130 86.6

T.P. 3.37 1190 08

12.87 1186.71

119

6.3 83.8

+50

10.3 79.8

120

13.0 77.1

T.P. 2.53 1179 77

12.84 1177.24

120+ 33'-20" Cor pipe

46 75.2

Reqd 24" Hillside

See stress forming on th. end,

(60" width would be enough)

121

7.8 72.0

T.P.

122

12.1 67.7

T.P. 3.81 1171 92

11.66 1168.11

123

8.1 63.8

23

+3.7 +3.6 -0.6 -2.0 -1.1 -0.5 0.0 -0.8 -1.7 -0.3 +1.2 +0.8
 $\frac{5.9}{25} \frac{6.0}{20} \frac{10.2}{15.4} \frac{11.6}{13} \frac{10.7}{12} \frac{10.1}{9} \frac{9.6}{8} \frac{10.4}{7} \frac{11.3}{6} \frac{9.9}{5} \frac{8.4}{4} \frac{8.8}{2.5}$

+4.2 +1.2 -0.6 -2.3 -0.6 -0.2 0.0 -0.9 -1.9 +1.8 +0.7
 $\frac{8.7}{25} \frac{11.2}{19} \frac{13.6}{18} \frac{15.3}{15.13} \frac{13.6}{12} \frac{13.2}{8} \frac{13.0}{8} \frac{13.9}{7} \frac{14.2}{9} \frac{11.2}{12} \frac{12.3}{2.5}$

+6.6 +6.3 +6.0 -2.0 -0.7 -0.1 +0.2 0.0 -0.8 -0.8 +3.9 +4.0
 $\frac{-0.3}{30} \frac{0.3}{26} \frac{8.3}{25} \frac{7.9}{17.15} \frac{6.4}{14} \frac{6.1}{7} \frac{6.3}{6} \frac{7.1}{6} \frac{8.1}{7.8} \frac{2.4}{14} \frac{2.3}{2.5}$

+7.3 +7.1 +2.8 -1.7 -1.0 -0.4 0.0 -0.8 -1.7 +5.5 +5.5
 $\frac{3.0}{25} \frac{3.2}{23} \frac{3.5}{17} \frac{12.0}{14.78} \frac{11.3}{12} \frac{10.7}{11} \frac{10.3}{8} \frac{11.1}{9.11} \frac{12.0}{7.8} \frac{4.8}{7.8} \frac{4.8}{2.5}$

+3.9 +3.7 -0.3 -1.2 -0.3 0.0 -1.3 -1.9 +0.1 +1.2 +3.2 +3.0
 $\frac{9.4}{25} \frac{9.6}{23} \frac{3.3}{14} \frac{14.2}{12.12} \frac{13.3}{10} \frac{13.0}{11} \frac{14.3}{11} \frac{14.7}{12.13} \frac{12.9}{14} \frac{13.3}{17} \frac{8.8}{21} \frac{10.0}{2.5}$

1173.9

-2.5
 $\frac{5.9}{FL} \frac{20.6}{FL}$

1172.4
 $\frac{+0.5}{FL} \frac{0.0}{FL} \frac{-1.1}{FL} \frac{-2.8}{FL} \frac{-2.6}{FL} \frac{-5.3}{FL}$

+5.7 +3.1 -0.2 -0.8 0.0 +0.2 0.0 -0.4 -0.6 +0.2 +1.1 +1.9 +1.2
 $\frac{4.0}{30} \frac{4.6}{25} \frac{7.9}{17} \frac{8.5}{16} \frac{7.7}{12} \frac{7.5}{3} \frac{1.7}{8} \frac{3.1}{8.9} \frac{3.3}{10} \frac{3.5}{10} \frac{5.5}{10} \frac{5.3}{17} \frac{6.5}{2.5}$

+5.0 +4.5 +0.8 -1.1 -0.6 +0.1 0.0 -0.9 -1.8 0.0 +1.9 +2.3 +2.1
 $\frac{7.1}{25} \frac{7.6}{21} \frac{11.3}{16} \frac{13.2}{14} \frac{12.7}{12} \frac{12.0}{3} \frac{12.1}{6} \frac{13.0}{8.9} \frac{13.9}{10} \frac{12.1}{10} \frac{10.2}{14} \frac{7.8}{14} \frac{19.0}{2.5}$

+3.5 +3.3 -0.9 -1.5 -0.8 +0.2 0.0 -0.5 -1.2 -2.3 -0.5 +1.0 +1.6 +1.5
 $\frac{4.6}{25} \frac{4.8}{21} \frac{9.0}{14} \frac{4.6}{13.12} \frac{8.9}{11} \frac{7.9}{3} \frac{8.1}{5} \frac{8.6}{8} \frac{9.3}{8} \frac{10.4}{4} \frac{7.4}{10} \frac{7.1}{14} \frac{6.5}{20} \frac{6.6}{2.5}$

1171 92

124			13.5	58.4
T.P.	2.17	1162	06	12.03 1159.89
+80			6.9	55.2
125			8.5	53.6
T.P.	0.12	1150	45	11.73 1150.3
126			5.9	44.6
+60			12.1	38.4
T.P.	2.97	1140	7.1	12.71 1137.74
127			5.2	35.5
J.M.			7.6	1132.94 1132.95
T.P.	1.06	1133	7.1	11.06 1129.65
128			4.3	29.4
+30			6.0	27.7
129			12.1	21.6
T.P.	1.44	1122	8.6	12.29 1121.42
+80			4.7	18.2
130			6.6	16.3

24

+4.1 +1.4 +0.4 -1.9 -0.5 +0.4 0.0 -1.2 -2.0 +2.0 +0.6				
$\frac{24}{25}$ $\frac{12}{19}$ $\frac{13}{15}$ $\frac{15}{13}$ $\frac{14}{11}$ $\frac{13}{3}$ $\frac{15}{7}$ $\frac{14}{9}$ $\frac{15}{11}$ $\frac{11}{25}$				
+4.6 +4.1				
$\frac{23}{30}$ +0.4 +0.3 -0.3 -2.6 -1.4 -0.6 0.0 0.0 -0.5 -1.7 +0.9 +0.8				
$\frac{22.5}{220}$ $\frac{25}{17}$ $\frac{25}{15}$ $\frac{22}{14}$ $\frac{23}{13}$ $\frac{24}{12}$ $\frac{25}{10}$ $\frac{26}{4}$ $\frac{27}{4}$ $\frac{28}{7}$ $\frac{29}{10}$ $\frac{30}{19}$ $\frac{31}{25}$				
+5.3 +5.2 +5.3 -0.9 -1.5 -0.4 0.0 -0.4 -0.9 -1.4 +1.1 +0.9 +0.8 +5 +1.0				
$\frac{32}{30}$ $\frac{33}{25}$ $\frac{32}{19}$ $\frac{34}{13}$ $\frac{100}{14}$ $\frac{87}{13}$ $\frac{85}{11}$ $\frac{27}{5}$ $\frac{24}{9}$ $\frac{29}{4}$ $\frac{28}{7}$ $\frac{24}{10}$ $\frac{20}{13}$ $\frac{21}{20}$ $\frac{20}{25}$				
+7.7 +7.1 +5.9 -1.1 -0.2 0.0 0.0 -0.3 -0.2 -0.3 +2.3 +2.7				
$\frac{1.3}{25}$ $\frac{1.2}{20}$ $\frac{0.0}{17}$ $\frac{2.2}{8.7}$ $\frac{6.1}{6}$ $\frac{5.9}{4}$ $\frac{5.1}{9}$ $\frac{6.2}{7}$ $\frac{7.1}{12}$ $\frac{6.3}{14}$ $\frac{3.2}{14}$ $\frac{3.2}{16}$ $\frac{3.2}{25}$				
46.9 +4.1 +3.4 +2.1 -0.3 -1.7 -0.1 0.0 -0.4 -1.8 -0.7 +2.6				
$\frac{52}{25}$ $\frac{51}{17}$ $\frac{49}{15}$ $\frac{10.9}{11}$ $\frac{12.4}{8}$ $\frac{13.8}{7.6}$ $\frac{12.2}{2}$ $\frac{12.1}{11}$ $\frac{12.5}{15}$ $\frac{13.9}{12}$ $\frac{12.5}{7.2}$ $\frac{9.5}{25}$				
+5.5 +4.7 +0.4 -1.5 -0.2 0.0 +0.1 -0.3 -1.2 -2.0 -0.6 +1.5				
$\frac{9.3}{25}$ $\frac{3.3}{20}$ $\frac{4.8}{13}$ $\frac{6.7}{8.5}$ $\frac{5.4}{3}$ $\frac{5.2}{2}$ $\frac{5.1}{2}$ $\frac{5.3}{11}$ $\frac{6.4}{15}$ $\frac{7.2}{16}$ $\frac{5.8}{17}$ $\frac{3.7}{25}$				
best spike in E. side H Apple 35' Rt. str. 127 + 85				
+5.7 +3.5 -1.0 -1.7 -1.0 -0.5 0.0 +0.3 -0.1 -0.4 0.0 +1.1 +1.2				
$\frac{7.4}{30}$ $\frac{0.8}{25}$ $\frac{5.3}{17}$ $\frac{6.0}{12}$ $\frac{6.0}{11.9}$ $\frac{5.3}{8}$ $\frac{4.7}{5}$ $\frac{4.3}{5}$ $\frac{4.0}{3}$ $\frac{4.4}{12}$ $\frac{4.2}{12.4}$ $\frac{4.3}{15}$ $\frac{3.2}{20}$ $\frac{3.1}{25}$				
+6.0 +4.4 -1.1 -2.7 -1.1 -0.3 0.0 +0.4 -0.2 -1.4 -0.1 +0.6 +0.8				
$\frac{6.0}{25}$ $\frac{6.4}{18}$ $\frac{7.1}{11}$ $\frac{5.7}{10.7}$ $\frac{7.1}{8}$ $\frac{6.3}{4}$ $\frac{6.0}{5}$ $\frac{5.6}{5}$ $\frac{6.8}{11}$ $\frac{7.4}{14}$ $\frac{6.1}{15}$ $\frac{5.4}{12}$ $\frac{5.2}{20}$ $\frac{5.2}{25}$				
+6.0 +6.1 +5.3 -0.7 -0.2 0.0 +0.2 -0.1 -0.9 -1.7 +0.5 +2.5 +5.3				
$\frac{6.1}{25}$ $\frac{6.0}{21}$ $\frac{6.3}{17}$ $\frac{12.3}{10}$ $\frac{12.3}{9}$ $\frac{13.1}{4}$ $\frac{11.9}{9}$ $\frac{12.7}{9}$ $\frac{13.0}{12}$ $\frac{13.8}{13}$ $\frac{11.6}{15}$ $\frac{9.6}{17}$ $\frac{6.3}{25}$				
+0.4 +0.1 0.0 0.0 -0.8 -1.3 -0.6 +1.7 +2.9				
Driveway $\frac{4.2}{20}$ $\frac{4.6}{24}$ $\frac{4.7}{4}$ $\frac{4.7}{4}$ $\frac{5.0}{9}$ $\frac{6.0}{10}$ $\frac{5.3}{11}$ $\frac{5.0}{10}$ $\frac{1.3}{25}$				
+2.4 +1.1 0.0 -0.1 -1.0 -0.7 -0.1 +2.2 +2.9				
$\frac{4.2}{25}$ $\frac{5.5}{10}$ $\frac{6.6}{7}$ $\frac{6.7}{7.1}$ $\frac{7.4}{10}$ $\frac{7.3}{11}$ $\frac{6.7}{14}$ $\frac{4.4}{21}$ $\frac{3.7}{25}$				

1122 ³86

130+50

110 11.9

T.P. 5.98 1116 ³28 12.56 1110.30
 131 8.2 08.1

+50 10.4 05.9

FF
 132 11.3 05.0

T.P. 328 1108 ⁹88 10.68 1105.60

+42 3'x2' Stone Box 4.3 04.6
 Good Cond.

133 6.2 02.7

134 8.3 00.6

B.M. 7.87 1100.99 1101.01

135 9.8 99.1

P.J. 10.6 98.3

25

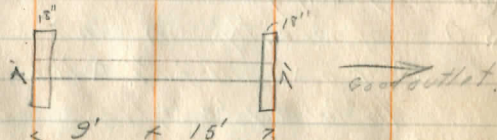
+6.4+6.3+1.9 +0.3 +0.8 0.0 -0.1 -0.5 -0.7 +0.9
 $\frac{41}{25} \frac{47}{24} \frac{91}{17} \frac{107}{15-14} \frac{102}{13} \frac{11.0}{7} \frac{11.1}{3-10} \frac{11.5}{11.2} \frac{11.7}{25} \frac{10.1}{25}$

+5.5 +4.5 -0.6 -1.4 -0.3 -0.6 0.0 +0.1 -0.3 -1.0 +0.3
 $\frac{27}{25} \frac{37}{20} \frac{8.8}{13} \frac{9.6}{12-11} \frac{8.5}{10} \frac{8.2}{7} \frac{8.2}{3} \frac{8.1}{8} \frac{8.5}{11-10} \frac{8.2}{19-2.5} \frac{7.9}{25}$

+2.5 0.0 -0.7 -0.1 -0.7 -0.3 0.0 +0.2 -0.5 -1.1 -0.3
 $\frac{29}{25-22} \frac{10.4}{15} \frac{111}{15} \frac{10.5}{11} \frac{11.1}{10-9} \frac{10.7}{7} \frac{10.4}{3} \frac{10.2}{13} \frac{10.7}{2.2} \frac{11.5}{2.5} \frac{10.7}{2.5}$

-0.9 -0.3 -0.5 0.0 0.0 0.0 -0.6 -1.5 -1.7
 $\frac{12.2}{25} \frac{11.6}{13} \frac{11.8}{11-10} \frac{11.3}{9} \frac{11.3}{4} \frac{11.2}{11} \frac{12.8}{14} \frac{13.0}{25}$

+1.9 +1.1 -1.1 -2.2 -3.4 +1.0 +0.4 0.0 0.0 +0.8 -3.8
 $\frac{24}{25} \frac{32}{32} \frac{5.4}{17} \frac{5.5}{13} \frac{6.7}{15} \frac{3.3}{9} \frac{3.1}{6} \frac{4.3}{4} \frac{4.3}{13} \frac{2.8}{14} \frac{8.1}{FL}$



+1.9 +1.8 +1.4 -0.5 -0.1 0.0 0.0 -0.5 -1.6 -0.5 -0.8
 $\frac{4.3}{25} \frac{4.4}{18} \frac{4.8}{11} \frac{6.7}{9} \frac{6.3}{7} \frac{6.2}{8} \frac{6.1}{12} \frac{7.8}{15-10} \frac{6.7}{18} \frac{7.0}{25}$

+0.7 +0.4 +0.2 -1.1 -0.5 0.0 +0.1 -0.5 -1.0 +1.0 +1.1
 $\frac{7.6}{25} \frac{7.7}{15} \frac{5.1}{12} \frac{5.4}{10} \frac{5.3}{8} \frac{8.3}{3} \frac{8.2}{9} \frac{8.8}{12} \frac{9.3}{15} \frac{7.3}{25} \frac{7.2}{25}$

+0.6 +0.5 -1.2 -0.6 0.0 0.0 -0.5 +0.7 +1.2

Nail with tin cap in W. root 21' Maple 30' Rk. sto, 134+80

$\frac{9.2}{25} \frac{9.3}{12} \frac{11.0}{11-10} \frac{10.4}{9} \frac{9.8}{9} \frac{9.8}{3} \frac{10.3}{11-13} \frac{9.1}{15} \frac{9.6}{2.5}$

+1.2 -0.3 -1.4 -0.8 -0.1 0.0 -0.4 +0.6 +0.9 +0.7
 $\frac{8.8}{25} \frac{10.3}{18} \frac{12.0}{15-14} \frac{11.3}{13} \frac{10.7}{4} \frac{10.6}{4} \frac{11.0}{10} \frac{10.0}{12} \frac{9.7}{21} \frac{9.9}{2.5}$

10-3-'22
Fair-Hot
Dusty

Hanno
Grad
Spohn

B.M.	151	1102	52	1100.99
136				5.4 97.1
				5.6 96.9
				7.4 95.1
137				6.0 96.5
138				6.3 96.2
(use for yardage)				
+50	apparently an old drain or box, all full & N.B.			6.2 96.3
				(12" pipe may be Regl.)
139				7.1 95.4
T.P.	3.54	1099	12	6.94 1095.59
140				3.2 95.9
+25				3.8 95.3
141				6.1 93.0
142				8.4 90.7
143				9.7 89.4
T.P.	3.62	1092	16	10.58 1088.54

+1.3	+0.4	-0.7	-0.4	0.0	+0.7	-0.1	+1.0
4.1	5.0	6.1	5.8	5.4	4.7	5.5	4.4
2.5	7.2	11.7	8		2.5	3.5	4.0

100' Rt. on oblique Rd.
200' " " " "

+0.5	+0.2	-0.7	0.0	+0.2	-0.3	-0.4	-0.2
5.5	5.8	6.7	6.0	5.3	6.3	6.4	6.2
2.5	7.4	12.10		4	7.9	2.5	4.0

-1.4	-0.5	-0.9	-0.7	-0.3	0.0	-0.5	-1.2	-0.4	-0.5
7.7	6.8	7.2	7.3	6.5	6.3	6.8	7.5	6.7	6.8
2.5	1.5	7.4	7.3	8		8	7.2	7.8	2.5

-1.4	-0.5	-1.1	0.0	+0.1	0.0	-0.6	-1.1	-0.6	-0.4
7.7	6.7	7.3	6.2	6.1	6.2	6.8	7.3	6.8	6.6
3.5	2.5	7.4	7.7	4	6.2	7	9.0	7.1	2.5

-0.3	-0.2	-0.9	-0.1	0.0	-0.4	-0.7	+0.5	+1.5	+2.4
8.0	7.3	8.0	7.2	7.1	7.5	7.8	6.5	5.6	4.7
2.5	7.5	7.4	5		7	7	7.1	7.5	2.5

+0.7	+0.1	-1.4	-1.8	-0.1	0.0	-0.7	-1.1	+1.1	+1.1	+0.8
3.3	3.1	4.6	4.0	3.3	3.2	3.7	4.3	2.1	2.1	2.7
2.5	7.2	7.4	7.1	4		2	8	7.1	2.1	2.5

+2.2	+1.8	+1.3	-0.9	-0.4	+0.1	0.0	-0.7	-1.1	+1.5	+1.3	+0.8
1.6	1.9	2.5	4.7	4.2	3.7	2.8	4.5	4.7	2.3	2.3	3.0
2.5	2.0	7.7	14.13	7.1	4		6	7	7.2	2.2	2.5

+3.2	+3.0	+1.1	-0.6	-0.3	0.0	0.0	-0.5	-0.9	+0.1	-0.5
2.7	3.1	5.0	6.7	6.4	6.1	6.1	6.6	7.0	6.0	6.6
2.5	7.0	15.15	7.0	7.1	5		7	8.9	7.0	2.5

+1.6	+0.6	-0.9	-0.5	0.0	0.0	-0.6	-1.0	-0.2	0.0
6.2	7.5	9.3	8.9	8.1	8.4	9.0	9.4	8.6	7.4
2.5	7.5	14.12	7.0	4		7	9	7.0	2.5

+0.3	-0.6	-0.9	-0.2	0.0	-0.8	-0.1	-0.5
2.4	10.3	10.1	8.9	9.7	10.5	9.8	10.2
2.5	7.4	15.11	4		4	7.1	2.5

✓

109216

144 3.7 88.5

145 4.0 88.2

146 4.3 87.9

+35 ? tile under Road. filled.

Regd. 12" pipe

147 4.0 88.2

148 1.8 90.4

T.P. 5.63 1095 48 2.31 1089.85

+35 4.5 91.0

149 4.0 91.5

J.M. 4.48 1091.00

150 4.0 91.5

151 6.3 89.2

152 7.1 88.4

153 7.0 88.5

No outlet for Lt. ditch & small sag
at 152 - Natural course to Rt. & Bacon's barn

27

+0.4	-0.2	-0.8	0.0	0.0	-0.4	-0.8
3.3	3.9	4.5	3.7	3.7	4.1	4.5
2.5	1.4	1.3	2	1.4	2.5	2.5

-0.4	-0.7	-1.0	-0.6	-0.1	0.0	-0.4	-0.9	0.0	-0.5
4.4	4.7	5.0	4.6	4.1	4.0	4.4	4.9	4.0	4.5
2.5	1.3	1.2	1.0	1.2	1.0	1.7	1.9	1.1	1.5-2.5

-0.4	-0.6	-1.1	-0.6	0.0	-0.4	-0.7	0.0	+0.3		
4.7	4.9	5.4	4.7	4.3	4.7	5.0	4.3	4.0		
2.5	1.3	1.2	1.0	1.0	1.7	1.0	1.1	1.5		
1087.4	1087.2	1086.9	1087.4	1087.8	1088.2	1087.6	1086.7	1085.8	1087.2	1087.3
-0.8	-1.0	-1.3	-0.8	-0.4	0.0	-0.6	-1.5	-2.4	-1.0	-0.7
4.8	5.0	5.3	4.8	4.4	4.0	4.6	5.5	4.4	5.0	4.9
2.5	1.9	1.2	1.1	1.4	1.0	1.8	1.0	1.6	1.5	2.5

-0.1	-0.9	-1.1	-0.8	-0.2	0.0	-0.7	-1.1	-0.8	-0.4
4.1	4.9	5.1	4.8	4.3	4.0	4.7	5.1	4.8	4.4
2.5	1.3	1.2	1.0	1.3	1.0	1.7	1.0	1.1	1.5

+0.8	+0.6	-0.8	-0.5	0.0	-0.2	-0.5	+0.5	+0.3
1.9	1.2	2.6	2.3	1.8	2.0	2.3	1.3	1.5
2.5	1.7	1.2	1.4	1.8	1.0	1.2	1.5	2.5

-0.1	-0.6	-1.0	-0.6	-0.1	0.0	-0.1	-0.8	0.0	-0.3
4.6	5.1	5.5	5.1	4.6	4.5	4.6	5.3	4.5	4.8
2.5	1.3	1.2	1.0	1.4	1.5	1.7	1.9	1.7	2.5

+0.9	+0.4	-0.3	-0.9	-0.4	0.0	-0.2	-1.1	-0.1	-0.8
3.1	3.6	4.3	4.9	4.4	4.0	4.2	5.1	4.1	4.8
2.5	1.6	1.2	1.1	1.4	1.0	1.2	1.0	1.1	1.5

Nail with cap in S. W. root 18" Maple 22" Rt. Sta. 1987+98

+0.7	+0.5	-0.2	-0.9	-0.5	0.0	-0.4	-1.0	-0.3	-0.8
3.3	3.5	4.2	4.9	4.5	4.0	4.1	5.0	4.3	4.8
2.5	1.8	1.2	1.1	1.4	1.0	1.7	1.0	1.1	1.5

+1.1	+0.8	0.0	0.0	0.0	+0.2	+1.0	+0.9	
5.7	5.5	6.3	6.3	6.3	6.1	5.3	5.4	
2.5	1.9	1.0	1.0	1.0	1.1	1.1	1.5	
1087.3	1087.4	1087.9	1087.2	1087.8	1088.2	1088.1	1087.6	
-1.1	-1.0	-0.5	-1.2	-0.6	-0.2	0.0	-0.3	-0.8
8.2	8.1	7.6	8.3	8.7	7.3	7.4	7.9	
2.5	1.8	1.0	1.4	1.7	1.4	1.4	1.5	

+0.9	+0.8	0.0	0.0	0.0	-0.6	-0.2
6.1	6.3	7.0	7.0	7.0	7.4	7.2
2.5	1.7	1.0	1.0	1.0	1.1	1.4-2.5

Take Lt. ditch water forward in Lt. ditch.

1095⁵48

+60

7.2 88.3

154

8.5 87.0

T.P. 3.65 1091 81

7.32 1088.16

155

10.3 81.5

154+50

7.4 84.4

T.P. 5.30 1085³ 27

11.84 1079.97

155+50

7.8 77.5

156

11.4 73.9

T.P. 1.27 1074⁶ 56

11.98 1073.29

157

7.7 66.9

158

13.0 61.6

T.P. 0.42 1062 23

12.75 1061.81

159

6.2 56.0

160

11.2 51.0

noon T.P. 1.26 1050 46

13.03 1049.20

161

3.5 47.0

162

6.6 43.9

Lt. ditch drains To Lts in sag

20

+1.2 +0.9 0.0 -0.7 -0.4 0.0 +0.1 -0.7 -0.2 -0.4
 $\frac{6.0}{2.5} \frac{6.3}{14} \frac{7.2}{7} \frac{7.9}{6} \frac{7.6}{4} \frac{7.2}{4} \frac{7.1}{5} \frac{7.9}{12} \frac{7.4}{13} \frac{7.5}{2.5}$

-1.1 -0.2 -1.3 0.0 +0.2 -0.1 -0.4 +1.2 +0.9
 $\frac{9.6}{25} \frac{8.7}{12} \frac{8.8}{7} \frac{8.5}{7} \frac{8.3}{4} \frac{8.6}{11} \frac{8.7}{13} \frac{7.9}{17} \frac{7.6}{2.5}$

-0.6 +1.0 +1.6 -1.0 -0.5 0.0 +0.2 -0.2 -1.4 -0.6 +0.8 +1.3 +1.1
 $\frac{10.9}{2.6} \frac{9.3}{15} \frac{8.7}{9} \frac{11.3}{6} \frac{10.9}{7} \frac{10.3}{4} \frac{10.1}{3} \frac{10.5}{7} \frac{11.7}{11} \frac{10.9}{12} \frac{10.9}{12} \frac{10.9}{12} \frac{10.9}{12} \frac{10.9}{12}$

-2.3 -1.1 -0.6 -1.0 0.0 +0.3 +0.1 -0.1 +1.0 +0.8
 $\frac{8.7}{2.5} \frac{8.5}{17} \frac{8.0}{7} \frac{8.1}{7} \frac{7.4}{7} \frac{7.1}{4} \frac{7.3}{10} \frac{7.5}{12} \frac{6.4}{2.0} \frac{6.6}{2.5}$

-0.8 +0.5 +0.8 -1.0 -0.3 0.0 0.0 -0.2 -1.1 -0.6 +1.3
 $\frac{8.5}{2.5} \frac{8.3}{12} \frac{7.0}{9} \frac{8.5}{6} \frac{8.1}{3} \frac{7.8}{4} \frac{7.5}{7} \frac{8.3}{7} \frac{8.7}{10} \frac{8.8}{12} \frac{8.5}{2.5}$

-1.1 -0.4 -0.2 -1.7 -0.6 0.0 +0.2 -0.2 -1.1 +2.7 +1.4
 $\frac{12.5}{2.5} \frac{11.8}{18} \frac{11.6}{9} \frac{13.1}{7} \frac{12.0}{3} \frac{11.4}{3} \frac{11.2}{7} \frac{11.6}{7} \frac{12.5}{10} \frac{12.7}{12} \frac{11.4}{10} \frac{11.4}{10} \frac{11.4}{10}$

+1.7 +1.8 +1.6 -1.1 0.0 0.0 +0.1 -0.4 -1.0 +1.3 +1.2
 $\frac{6.0}{2.5} \frac{5.8}{17} \frac{6.1}{9} \frac{5.8}{7} \frac{7.7}{2} \frac{7.7}{4} \frac{7.6}{4} \frac{8.1}{9} \frac{8.7}{11} \frac{8.4}{12} \frac{8.4}{18} \frac{8.4}{21} \frac{3.5}{2.5}$

+2.7 +2.4 +1.5 -0.9 -0.5 0.0 +0.2 -0.5 -1.6 -0.5 +1.8 +1.4 +2.2
 $\frac{10.3}{2.5} \frac{10.4}{15} \frac{11.5}{9} \frac{13.7}{6.5} \frac{7.5}{4} \frac{7.5}{4} \frac{13.9}{4} \frac{12.8}{4} \frac{13.5}{10} \frac{14.6}{12} \frac{13.5}{13} \frac{11.2}{16} \frac{11.4}{20} \frac{10.3}{2.5}$

+2.6 +1.7 +0.4 -1.1 -0.6 0.0 +0.1 -0.7 -1.4 +2.0 +1.9 +1.3 +2.1
 $\frac{9.6}{2.5} \frac{4.3}{18} \frac{5.8}{10} \frac{7.3}{7} \frac{6.8}{5} \frac{6.2}{3} \frac{6.1}{5} \frac{6.9}{11} \frac{7.6}{12} \frac{4.2}{13} \frac{4.3}{16} \frac{4.9}{19} \frac{9.1}{22}$

+3.1 +2.9 +2.0 -1.0 -0.6 0.0 +0.3 -0.5 -1.4 +1.5 +0.7 +1.6
 $\frac{8.1}{2.5} \frac{8.3}{17} \frac{9.2}{9} \frac{12.7}{6.5} \frac{11.8}{4} \frac{11.2}{4} \frac{10.9}{4} \frac{11.7}{11} \frac{12.5}{13} \frac{11.7}{16} \frac{9.7}{19} \frac{10.5}{20} \frac{9.6}{2.5}$

+2.4 +1.6 +0.1 -1.3 -1.0 0.0 +0.1 -0.3 -0.7 -0.5 -0.2
 $\frac{11}{2.5} \frac{1.9}{17} \frac{3.4}{9} \frac{4.8}{7} \frac{4.5}{3} \frac{3.5}{3} \frac{3.4}{5} \frac{3.8}{10} \frac{4.2}{12} \frac{4.0}{15} \frac{3.7}{2.5}$

+0.9 +0.3 -0.1 0.0 -0.5 0.0 +0.3 -0.1 -0.1 +0.5
 $\frac{5.7}{2.5} \frac{6.3}{12} \frac{6.7}{15} \frac{6.6}{8} \frac{7.1}{6.4} \frac{6.6}{4} \frac{6.3}{5} \frac{7.0}{16} \frac{6.7}{13} \frac{6.1}{13} \frac{6.1}{13} \frac{6.1}{13} \frac{6.1}{13}$

1050 ⁵ 46

163			8.6	41.9
T.P.	2.48	1044	13	8.81 1041.65
164			3.6	40.5
+30			5.2	38.9
165			9.6	34.5
T.P.	0.52	1032	74	11.91 1032.22
166			3.4	29.3
167			6.9	25.8
168			9.5	23.2
J.M.	2.91	1025	8.3	9.82 1022.94
169			4.6	21.2
170			6.8	19.0
170+30			7.9	17.9

168+145 Possible location for
 a 12" Hillside pipe Coly.
 may need tile to Lt. for outlet.
 (270' from Lt.) (If pipe is not used open ditch 100' Lt.)

-2.9	-2.7	-1.5	-0.6	0.0	+0.1	-0.1	-0.6	-0.5	+0.6
11.5	11.3	10.1	9.2	8.6	8.5	8.7	9.2	9.1	8.0
2.5	1.8	8	6	5	5	11	12-13	14	2.5
+1.4	+0.7	-0.7	0.0	+0.2	-0.9	-1.9	+1.4	+1.5	
2.2	2.9	4.3	3.0	3.4	4.5	5.8	2.1	2.1	
2.5	1.5	6	5	5	12	14	17	2.5	
+2.5	+1.8	-0.7	-0.3	0.0	+0.5	-0.3	-1.4	+2.1	
2.7	3.4	5.7	5.5	5.7	4.7	5.5	6.6	3.1	
2.5	1.6	9	5	4	5	12	14-15	20-25	
+4.6	+4.3	+3.6	-0.7	-0.2	0.0	+0.3	-0.6	-1.4	+3.3 +3.0
5.0	5.3	6.9	10.3	9.8	9.6	9.3	10.2	11.0	6.3 6.5
2.5	2.0	10	4	3	2	12	13-14	20	2.5
+2.8	+2.5	+1.4	-0.9	-0.4	0.0	+0.5	-0.3	-1.6	+0.8 +1.9
0.6	0.9	2.0	4.3	3.8	3.4	2.9	3.7	5.0	2.0 1.5
2.5	1.5	7	5-7	3	5	12	15	18	2.5
-0.3	-0.1	0.0	-1.1	-0.5	0.0	+0.5	-0.3	-0.8	+0.4 +1.6
7.3	7.0	6.9	8.0	7.4	6.7	6.4	7.2	7.7	6.8 5.3
2.5	1.7	7	6-5	3	4	7	11	13-14	16 2.5
-1.7	-0.8	+0.1	-0.7	-0.4	0.0	+0.2	-0.3	0.0	-0.1 +0.4 +1.5
11.2	10.3	9.4	10.2	9.2	9.5	9.3	9.8	9.5	9.0 8.0
2.5	1.5	7	6	3	3	6	11	14	15 2.5
Bottom J.E. Cor. board house Lt. 574 164+15									
+0.6	+0.3	-0.6	-0.3	0.0	+0.5	-0.2	-1.0	+1.1	+1.0
4.0	4.3	5.2	4.9	4.6	4.1	4.5	5.6	3.5	3.5
2.5	2	8-4	3	4	11	13	15	2.5	
+1.3	+0.9	+0.1	-1.3	-0.6	0.0	+0.2	-0.8	-1.4	+1.2 +0.6
5.5	5.7	6.7	8.1	7.4	6.7	6.6	7.6	8.2	5.6 6.2
2.5	1.7	7	6	4	3	7.5	12-13	14	2.5
+2.2	+2.4	+2.0	+1.1	+0.9	-1.5	-0.4	0.0	+0.1	-0.8 -1.3 +1.7 +1.1
5.7	5.5	5.7	6.8	7.0	6.4	6.3	7.9	7.8	8.7 9.2 6.2 6.3
2.5	2.1	14	12	9	8.7	4	6	10	12-13 15 2.5

1018.5
 1020.8
 1021.7
 1021.4
 1021.4
 1021.8
 1022.3
 1022.6
 1022.3
 1021.6
 1022.8
 1023.1

-3.8	-1.5	-0.6	1.0	-0.9	-0.5	0.0	1.0	0.0	-0.7	+0.5	+0.8
7.3	5.0	4.1	3.4	4.4	4.6	3.3	3.1	3.3	4.2	5.0	2.7
5.3	2.5	1.6	7	6.5	4	3	4	11	12-13	16	2.5

10-19-22
Fair-cold

J.M. 0.96 1023 88 1022.92

171 9.8 14.1

T.P. 30.5 1015 01 11.92 1011.96
+65 5.3 09.7

172 9.4 06.6

T.P. 0.55 1002 94 12.62 1002.39

173 4.6 98.3

T.P. 0.38 990 35 12.97 989.97

174 2.1 88.3

T.P. 0.52 978 46 12.41 977.94

175 1.8 76.7

T.P. 0.41 966 73 12.14 966.32

176 3.5 63.2

177 0.85 955 32 12.26 954.47

4.4 50.9

T.P. 2.86 945 42 12.76 942.56
177+50 3.5 41.9

178 11.0 34.4

T.P. 0.31 939 15 12.58 937.84

Hanna
Grau
Spohn

30

+3.7 +2.7 +0.9 -1.9 -1.3 -0.4 0.0 -0.6 -1.2 -2.4 +2.6 +2.7
5.1 7.1 9.4 11.7 14.1 16.2 18.2 19.4 11.0 12.7 14.7 16.1
25 15 11 10 9 7 5 10 12 14 15

+3.5 +3.8 +1.9 -2.1 -1.3 -0.3 0.0 -0.6 -1.2 +2.1 +2.5 +2.3
1.8 1.5 3.4 7.4 6.6 5.6 5.3 5.9 6.3 3.2 2.8 3.0
2.5 2.0 1.4 1.1 1.0 1.2 1.5 1.7 2.5

+4.6 +4.8 +2.9 -0.8 -0.3 0.0 -0.2 -1.0 -1.8 +1.2 +3.4 +3.6
3.9 3.6 5.5 3.2 8.7 8.4 9.6 9.4 10.2 7.5 3.0 4.8
2.5 2.1 1.5 1.2 1.3 1.1 7 10 11 13 17 2.5

+6.8 +6.6 +2.7 +1.0 -1.1 -0.7 -0.1 0.0 -0.2 -0.7 -1.5 +5.8 +4.4 +5.8
-2.3 -2.0 1.8 3.6 5.7 5.3 4.7 4.6 4.8 5.3 6.1 1.2 1.5 1.2
2.5 2.1 1.7 1.4 1.3 1.2 1.1 1.1 1.2 1.4 1.4 1.4 1.4 2.5

+9.8 +10.3 +9.9 -1.9 -0.9 +0.2 0.0 -0.7 -1.5 -2.7 +8.5 +8.3
-7.7 -9.2 -7.8 4.8 3.0 2.3 1.2 2.1 2.8 3.5 4.8 2.4 1.2
3.0 2.5 2.3 1.3 1.2 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 2.5

130 +8.0 +12.4 +3.7 +2.9 -1.2 -0.5 0.0 0.0 -0.7 -1.2 +1.4 +5.2 +10.8 +10.2
-11.2 -1.0 1.9 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1
2.0 2.9 2.5 1.7 1.5 1.2 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1

+12.3 +12.0 +3.5 -1.3 -0.1 0.0 0.0 -0.3 -0.8 -1.3 -2.5 +0.8 +3.5 +5.6 +10
-8.8 -9.5 0.0 4.8 3.6 3.5 3.5 3.8 4.3 4.8 6.0 3.1 0.0 -2.1 -2.5
2.5 2.3 1.5 1.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0

+3.1 +2.0 -0.9 +0.3 0.0 -0.3 -1.0 -2.2 +2.3 +2.5 +2.6
1.3 2.4 5.3 4.1 4.4 4.7 5.6 6.6 2.1 1.9 1.8
2.5 1.8 1.4 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1

10" V.Pipe under DW Lt

+2.1 +1.5 +0.5 -1.1 +0.1 0.0 -0.1 -1.9 +0.1 +1.7 +3.1
1.4 2.0 3.0 4.6 3.4 3.5 3.6 5.4 3.4 1.8 0.4
2.5 2.1 1.8 1.7 1.6 1.6 1.6 1.6 1.6 1.6 1.6

-3.0 -2.5 -1.1 -0.5 -0.8 -0.4 +0.1 0.0 -0.3 -0.1 -0.7 +0.4 -0.2
1.4 1.5 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1
2.5 2.0 1.6 1.2 1.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0

15" V.Pipe in D.W. to Rt

933 15

178+50 4.0 29.2

+65 4.9 28.3

179 7.0 26.2
 J.M. 10.90 934 14 9.71 $\frac{923.25}{923.24}$

+50 8.9 25.2

770 8.6 25.5

27.8 906.3

180 8.1 26.0

+50 6.0 28.1
 T.P. 9.04 942 10 1.08 933.06

181 8.8 33.3

-3.2 -2.6 -2.2 -0.5 +0.1 0.0 +0.3 +0.1 2.0 -0.1
 $\frac{73}{25} \frac{66}{11} \frac{62}{13} \frac{45}{9} \frac{39}{6} \frac{10}{9} \frac{37}{9} \frac{32}{19} \frac{40}{25} \frac{41}{30}$

-3.1 -2.8 -1.6 -0.6 0.0 0.0 -0.2 -0.6 -1.1
 $\frac{80}{25} \frac{77}{17} \frac{65}{12} \frac{53}{6} \frac{17}{2} \frac{49}{7} \frac{51}{7} \frac{53}{12-17} \frac{60}{25}$

-6.6 -7.1 -7.9 -7.1 -3.7 -0.4 0.0 -0.2 -1.0 -3.7 -5.8 -11.5 -9.4
 $\frac{136}{30} \frac{141}{25} \frac{149}{22} \frac{141}{17} \frac{107}{13} \frac{74}{9} \frac{70}{6} \frac{72}{6} \frac{80}{9} \frac{107}{12} \frac{128}{15} \frac{145}{23-25} \frac{161}{27}$

x on N.W. Cor. Lt. wall to Arch bridge 179+68

-1.7 -0.5 -0.1 0.0 -0.3 -0.5 -1.8
 $\frac{106}{12.5} \frac{94}{10-8} \frac{90}{2} \frac{87}{1} \frac{84}{8} \frac{107}{12}$ wall steep

-17.1 -13.2 -7.1 -3.6 -2.2 -1.0 0.0 0.0 -0.3 -0.6 -1.6 -3.0 -5.4
 $\frac{257}{35} \frac{218}{28} \frac{157}{13} \frac{123}{14} \frac{108}{12} \frac{96}{10} \frac{89}{3} \frac{86}{3} \frac{82}{2} \frac{82}{9} \frac{102}{10} \frac{116}{14} \frac{140}{15.16}$

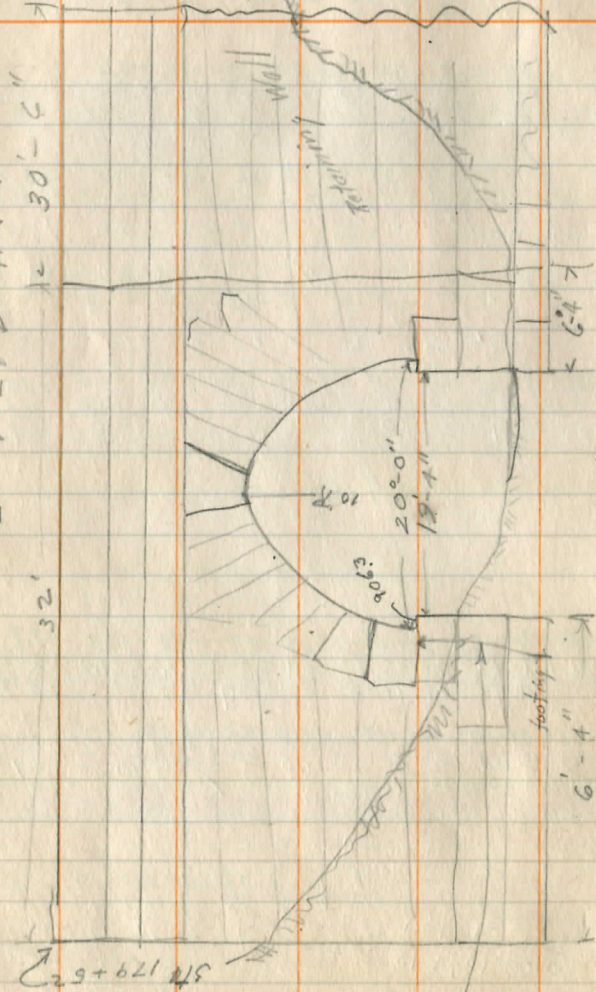
Elev. seat of arch

-13.6 -13.0 -10.0 -4.9 -2.9 -0.7 -0.5 0.0 -0.3 -4.9 -11.9 -17.7 -20.4 -21.7
 $\frac{212}{35} \frac{211}{30} \frac{181}{24} \frac{130}{16} \frac{110}{14} \frac{88}{11} \frac{84}{9} \frac{81}{9} \frac{84}{9} \frac{130}{15} \frac{260}{25} \frac{295}{32} \frac{298}{34} \frac{298}{37-40}$

-11.9 -10.9 -7.0 -5.3 -0.2 -1.0 -0.4 0.0 -0.2 +0.6 +2.3 -1.9 -7.0 -12.6 -12.9
 $\frac{179}{40} \frac{169}{31} \frac{130}{24} \frac{113}{20} \frac{62}{12-18} \frac{70}{9} \frac{64}{6} \frac{60}{6} \frac{62}{3} \frac{54}{7} \frac{48}{8-10} \frac{7.9}{15} \frac{130}{21} \frac{136}{30} \frac{129}{40}$

-6.3 -5.4 -4.2 10.4 11.7 10.7 -0.2 +0.1 0.0 -0.2 +0.3 +0.1 -1.0 0.0 +0.1 2.4 -4.2
 $\frac{151}{35} \frac{142}{30} \frac{130}{25} \frac{84}{18} \frac{74}{14} \frac{81}{13} \frac{90}{4} \frac{87}{4} \frac{90}{4} \frac{85}{7} \frac{87}{11} \frac{9.7}{12-13} \frac{29.4}{14.78} \frac{112}{25} \frac{120}{28}$
 -4.2 -14.5 -15.1
 $\frac{130}{30} \frac{20.3}{45} \frac{23.9}{50}$

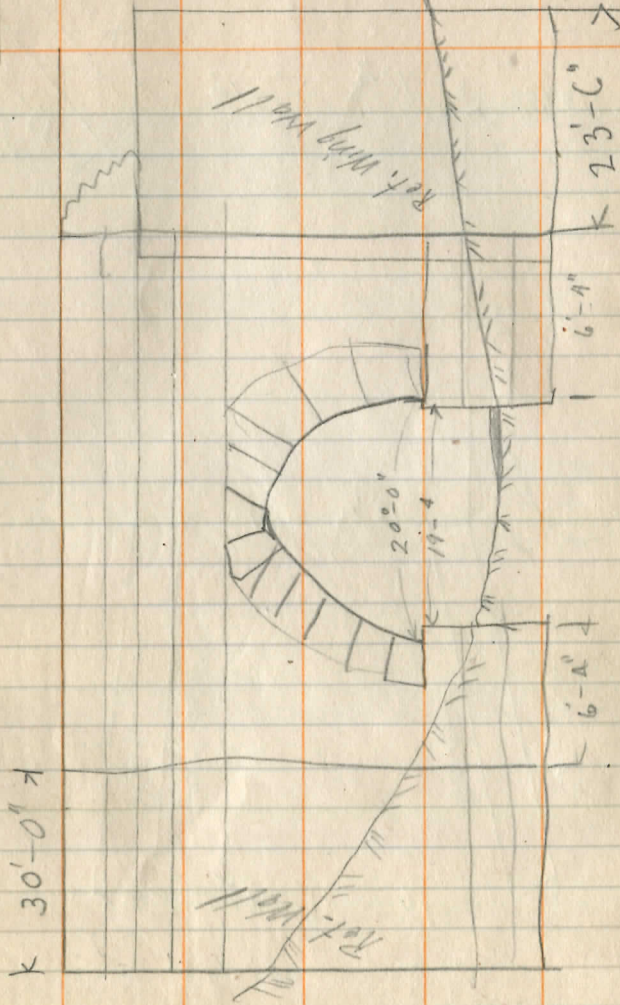
VIEW OF LEFT END ARCH



Elev. bot. Creek = 902.5

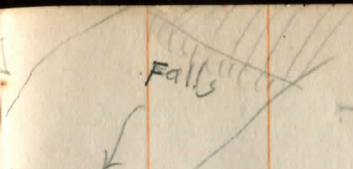
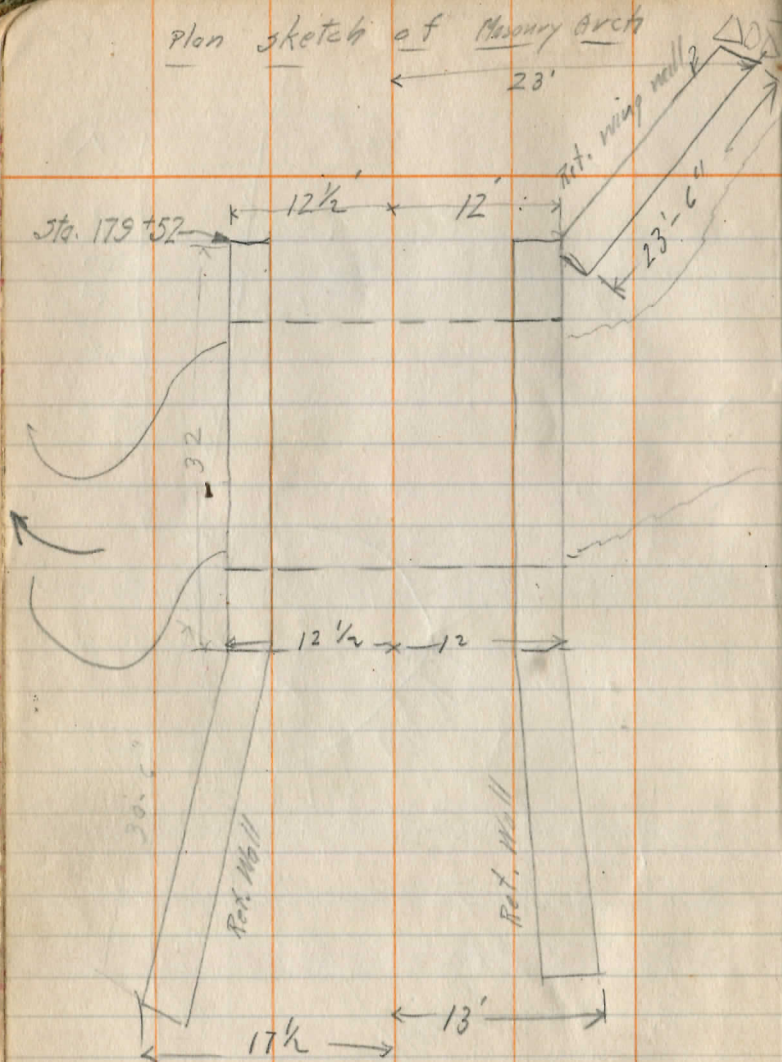
(About 4 1/2 ft)

VIEW OF RIGHT END ARCH



Masonry in Good Cond.

Plan sketch of Masonry Arch



10-20-22
Beautiful

10000
2000
3000

942.10

181+50

36 38.5

T.P. 10.98 952 87 021 941.89
182 7.7 43.2

183 3.0 49.9

T.P. 12.85 961 74 398 948.89

184 2.6 59.1

T.P. 10.90 972 10 0.54 961.20

185 5.0 67.1

T.P. 12.40 984 39 0.11 971.99

186 9.1 75.3

187 0.9 83.5

T.P. 11.27 995 02 0.64 993.75

+30 9.6 85.4

188 7.7 87.8

189 3.9 91.1

190 1.3 93.7

T.P. 10.20 1004 30 0.92 994.10

37

+55
-0.7 -0.5 -1.2 -0.4 +0.1 -0.3 0.0 +0.5 +0.3 -0.6 +2.8 +3.3 +5.3 -1.7
4.3 11 13 10 3.5 3.5 3.6 3.1 3.3 4.2 0.8 0.3 -1.7
2.5 17 15 16 2 8 5 8 10-11 14 18 24-25

-0.4 -0.5 -1.0 -1.2 -0.5 0.0 0.0 -0.2 +0.3 -0.5 +0.2 +2.6 +4.5 +4.9
10.1 10.2 10.7 10.9 10.2 9.7 9.7 9.9 9.4 10.2 9.3 7.1 5.2 4.8
2.5 2.1 1.6 1.5 1.3 5 5 9 10-11 12 15 20 25

+3.8 +3.1 +2.5 -0.4 -1.2 -0.6 0.0 0.0 -0.3 -1.3 0.0 +5.0 +5.8 +5.4
-0.1 -0.1 0.5 3.4 4.2 3.6 3.9 3.0 3.3 4.3 3.0 -2.0 -2.8 -2.4
2.5 2.3 1.7 1.3 1.2 1.0 2 1.0 11-12 13 19 22 25

3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00 3.00
+4.2 +2.6 -0.8 -0.4 -0.5 0.0 -0.1 +0.2 -0.6 +0.9 +2.6 +5.9
-1.1 0.0 3.4 3.0 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6
2.5 2.1 1.7 1.4 1.0 4

+5.4 +5.0 +1.0 -0.5 -1.4 -0.7 -0.4 0.0 -0.3 -1.0 +3.3 +6.2
-0.4 0.0 4.0 5.5 6.4 5.7 5.1 5.0 5.3 6.0 4.7 -1.2
2.5 2.0 1.3 1.0 0.8 7 2 1.0 11-12 13 2.5

+5.2 +5.1 +4.2 +1.4 -0.7 -0.3 0.0 -0.5 -1.9 +4.2 +6.6
3.2 3.0 4.2 2.7 2.8 2.1 2.1 2.6 1.0 4.4 2.5
2.5 2.1 1.8 1.1 9 8 3 7-11 19 2.5

+1.1 +0.5 -0.7 -1.1 -0.6 0.0 -0.1 -1.2 +0.8 +2.7 3.2
-0.2 0.4 1.6 2.0 1.5 0.8 1.0 3.1 0.1 -1.1 -2.3
2.5 1.6 1.2 1.1 1.0 1.0 1.2 1.4 1.7 2.5 2.5

0.0 -0.3 -1.4 -0.8 -0.5 0.0 -0.3 -1.2 -2.1 +0.8 +1.9 +2.3
9.6 9.7 11.0 10.9 10.1 9.6 9.7 10.3 11.7 5.8 3.7 2.3
2.5 1.7 1.4 1.3 1.1 1.0 1 1.3 1.4 1.7 2.5 2.5

+0.1 -0.5 -0.8 -0.5 0.0 -0.4 -0.3 -1.3 +0.1 +1.4
7.1 7.7 8.0 7.7 7.7 7.6 7.5 8.5 7.1 5.8
2.5 1.1 1.0 5 7 10 11-12 16 2.5

+1.2 +0.7 -0.7 0.0 -0.3 -1.3 +0.3 +2.2
2.7 3.2 4.6 3.9 4.3 5-10 6-11 3.6 1.7
2.5 1.4 8 12-14 17 2.5

+0.2 -0.4 0.0 -0.6 -0.2 -0.1 +0.4
1.1 1.7 1.3 1.4 1.5 1.4 0.8 0.8
2.5 1.3 11-6 10 13 2.8 2.5

✓

1004.30

191 9.3 95.0

192 7.9 96.4

193 5.8 98.5

194 3.6 00.7

B.M. 0.26 1004.03

T.P. 8.70 1011.00 2.00 1007.30

195 8.4 02.6

+60 12" Carr. Pipe 20' long 6.7 04.3
Reg'd 12" Hillside

196 5.7 05.8

197 1.5 09.5

T.P. 12.68 102.3 31 0.37 1010.63

198 6.7 16.6

+60 1.6 21.7

T.P. 11.66 1034 17 0.80 1022.5

35

-1.1	-0.5	-0.4	-0.1	0.0	-0.2	+0.3	+0.7	+0.8
10.4	9.8	9.7	9.4	9.3	9.5	9.0	8.6	8.5
25	18	12	4	43	11	13	19	25

take Lt. ditch water
to Lt.

-0.9	+0.3	-0.3	+0.1	0.0	-0.1	+0.9	+2.5	+2.0
8.8	7.6	8.2	7.8	7.9	8.0	7.0	5.4	5.9
30	13	7	4	7	9	13	20	25

+2.4	+2.0	+1.1	+0.9	-0.9	-0.4	0.0	0.0	-0.5	+0.4	+1.4	+2.2
3.4	3.3	4.7	4.2	6.7	6.2	5.3	5.8	6.3	5.4	4.4	3.6
25	21	19	15	12	10	3	5	8	12	16	25

+1.5	+1.4	+0.9	-0.5	-0.2	0.0	0.0	-0.4	-0.3	-0.9	-2.0
2.1	2.2	2.7	1.1	3.9	3.5	3.6	4.0	3.7	4.5	5.5
25	19	12	14	11	3	7	9	14	25	25

2
Two headed tock N.E. root 18" Maple 30' Lt. 1994

+0.8	-0.2	-0.5	-0.1	+0.1	0.0	-0.3	-0.4	-0.9	-2.5	-3.0
7.5	9.6	8.9	8.5	8.3	8.4	8.7	8.2	8.3	10.9	11.4
25	17	16	11	10	5	8	12	21	25	25

+0.4	+0.5	-1.6	-1.6	+0.2	-0.2	+0.1	0.0	-0.3	-2.3	-3.8	-3.9
6.3	6.2	8.3	8.3	6.5	6.9	6.6	6.7	8.0	8.0	10.5	10.5
20	14	7	4	11	9	8	2	8	15	23	23

(all is 1' show)

+2.6	+2.1	+0.1	-0.2	-1.1	-0.1	-0.7	-0.3	+0.2	0.0	-0.5	-1.1	-0.5	-0.3	-1.0	-1.4
6.3	5.7	5.4	6.3	5.3	5.9	5.5	5.0	5.2	5.7	6.3	5.7	5.5	6.2	6.6	6.6
25	17	14	13	10	7	6	2	6	8	7	10	11	16	23	25

+6.2	+4.6	+0.6	-0.3	-1.1	-0.5	-0.2	0.0	-0.3	-0.5	-1.2	-0.4	+1.3	+0.5	
4.7	3.1	0.9	1.3	2.6	2.0	1.7	1.5	1.8	2.0	2.7	1.9	0.2	1.0	
25	22	16	14	13	11	10	10	3	10	12	13	17	21	25

+4.6	+4.4	+2.6	-0.8	-0.4	0.0	0.0	-0.4	-0.7	-1.5	+0.6	+1.5	+1.6	
2.1	2.3	4.1	2.5	7.1	6.7	6.1	7.1	7.4	8.2	6.1	5.2	5.1	
25	22	19	15	10	6	3	6	10	11	12	15	17	25

+2.7	+2.9	+1.0	-2.1	-1.0	-0.4	0.0	-0.7	-1.9	+1.1	+0.4	
1.1	1.3	0.6	3.7	2.6	2.0	1.6	2.3	3.5	0.5	1.2	
25	22	15	15	12	11	9	9	12	13	17	25

1034 ² 17

199			9.7	24.5
200			1.6	32.6
T.P.	12.75	1046	0.05	1034.12
201			6.5	40.4
+40			4.1	42.8
T.P.	12.16	1058	0.33	1046.54
202			10.0	48.7
+40			6.0	52.7
203			2.0	56.7
T.P.	11.11	1069	0.62	1058.08
204			3.5	63.7
T.P.	10.80	1079	0.62	1068.57
205			8.3	71.1
T.				
206			0.4	79.0
T.P.	12.01	1091	0.14	1079.23
207			5.0	86.2
T.P.	6.34	1096	1.54	1089.10
B.M.			2.21	1093.83

+3.8	+3.2	+0.9	-1.4	-0.6	-0.4	0.0	-0.6	-1.9	-0.5	+0.1	-0.7	-0.2		
59	65	88	41	10.3	10.1	97	10.3	11.6	10.2	5.6	10.4	99		
25	20	15	13	12	10	6	7	9	40	11	18	21	25	
+4.0	+3.6	-1.1	-0.2	0.0	-0.6	-0.7	-1.5	-0.5	+1.2	+3.0	+2.9			
-2.4	-2.0	2.7	1.8	1.6	2.2	2.3	3.1	2.1	9.4	-1.4	-1.3			
25	18	11	12	9	4	10	11	12	14	22	25			
+2.1	+2.5	+0.4	-0.5	-0.3	0.0	0.0	-0.7	-1.6	+4.8	+5.4				
4.4	3.0	6.1	7.0	6.8	6.5	6.5	7.2	8.1	1.7	1.1				
25	17	13	11	9	3	12	14	15	22	25				
+4.8	+4.6	+4.1	-0.7	-0.3	0.0	0.0	-0.3	-1.0	-6.9	+6.6				
-0.7	-0.5	0.0	1.7	4.4	4.1	4.1	4.4	5.1	6.0	-2.5				
25	17	16	11	9	3	10	12	13	14	15	25			
+2.6	+3.6	-1.4	-0.3	0.0	0.0	0.0	-0.6	-0.4	-2.8	-0.5	+4.0	+4.4		
7.4	6.4	11.4	10.3	10.0	10.0	10.0	10.6	10.4	12.8	15.5	6.0	5.6		
25	16	11	8	10	2	7	10	11	12	13	19	25		
+0.1	+0.8	+2.4	-1.3	-0.6	0.0	0.0	-0.3	-1.6	+3.1	+3.5				
5.2	5.2	3.6	7.3	6.6	6.0	6.0	6.3	7.6	2.9	2.5				
25	21	17	15	14	8	3	10	11	12	19	25			
+1.0	+1.2	+2.3	+2.6	-1.6	0.0	+0.1	-1.0	-1.5	+3.7	+3.9				
1.0	0.8	-0.3	-0.6	3.6	2.0	1.9	3.0	3.5	1.7	1.7				
25	22	18	15	10	2	10	11	12	19	25				
+2.2	+2.4	+3.1	-1.1	-0.6	0.0	-0.7	-0.8	-1.5	+3.4	+3.8				
3.3	3.1	2.4	6.6	6.1	5.5	6.2	6.3	7.0	2.1	1.7				
23	21	16	12	11	9	6	9	10	11	13	25			
+2.5	+2.7	-1.3	-0.8	0.0	-0.5	-0.7	-1.2	+2.9	+3.5					
5.4	5.6	2.6	9.1	8.3	8.0	8.0	8.0	8.5	5.4	4.8				
25	19	11	10	9	4	8	9	10	15	25				
+3.5	+3.6	+1.9	+1.2	-1.0	0.0	-0.1	-1.8	-1.5	+1.4	+1.7	+3.1	+3.4		
-3.1	-3.7	-1.5	-0.8	1.4	0.1	0.5	1.2	1.9	-1.0	-1.3	-2.7	-3.0		
24	14	14	11	9	0.1	2	9	11	12	14	17	21	25	
+2.8	+2.6	+2.8	+3.3	+0.1	-0.9	-0.6	0.0	+0.1	-0.5	-0.8	+3.2	+4.2	+4.0	
2.2	2.4	2.7	1.7	1.2	5.4	5.4	5.0	4.9	5.5	5.8	1.8	0.8	1.0	
25	23	17	14	9	8	7	5	3	9	10	11	16	18	25

Tin headed tack w. root 15" Maple Rt. front of empty house

1096 04.

207+85

42 91.8

208

44 91.6

209

63 89.7

+94'

100' C.P. sec.
15" corr pipe {22' long
(Repd. 15. Pipe)

60 90.0

210

60 90.0

211

45 91.5

T.P. 11.93 1104 13

3.84 1092.20

212

92 94.9

213

2.6 01.5

T.P. 11.10 1114 91

0.32 1103.81

214

7.5 07.4

+50

49 10.0

37

$$\begin{array}{r} +0.1 \ +0.4 \ +0.8 \ -0.5 \ 0.0 \ -0.3 \ +1.6 \ +1.9 \\ \hline 41 \ 38 \ 34 \ 47 \ 42 \ 45 \ 26 \ 23 \\ \hline 25 \ 13 \ 10 \ 7 \ 8 \ 19 \ 25 \end{array}$$

$$\begin{array}{r} -0.6 \ -0.3 \ -0.8 \ -0.3 \ 0.0 \ -0.2 \ +0.2 \ +1.6 \\ \hline 43 \ 45 \ 50 \ 45 \ 44 \ 45 \ 40 \ 26 \\ \hline 25 \ 21 \ 10 \ 7 \ 1 \ 7 \ 14 \ 21 \ 25 \end{array}$$

$$\begin{array}{r} -0.7 \ -0.4 \ -0.9 \ -0.6 \ -0.5 \ +0.1 \ 0.0 \ -0.4 \ +0.5 \ +0.8 \\ \hline 70 \ 67 \ 72 \ 62 \ 68 \ 62 \ 63 \ 67 \ 58 \ 55 \\ \hline 25 \ 14 \ 13 \ 12 \ 8 \ 4 \ 6 \ 6 \ 17 \ 25 \end{array}$$

$$\begin{array}{r} 1086.6 \ 1087.5 \ 1089.3 \ 1090.0 \ 1090.1 \ 1089.0 \ 1088.5 \ 1089.0 \\ \hline -3.4 \ -2.5 \ -0.7 \ +0.1 \ 0.0 \ +0.1 \ -2.1 \ -1.5 \ -1.0 \\ \hline 94 \ 85 \ 67 \ 57 \ 60 \ 59 \ 81 \ 75 \ 70 \\ \hline 25 \ 14 \ 12 \ 7 \ 8 \ 14 \ 13 \ 25 \end{array}$$

$$\begin{array}{r} -2.1 \ -2.0 \ -1.1 \ -1.4 \ -0.5 \ +0.3 \ 0.0 \ -0.2 \ -1.2 \ -0.7 \ -0.8 \\ \hline 81 \ 80 \ 71 \ 74 \ 65 \ 57 \ 60 \ 62 \ 72 \ 67 \ 68 \\ \hline 25 \ 20 \ 14 \ 13 \ 11 \ 3 \ 6 \ 9 \ 10 \ 25 \end{array}$$

$$\begin{array}{r} -0.8 \ -1.1 \ -0.6 \ +0.2 \ 0.0 \ -0.9 \ -0.8 \ -0.2 \ +0.1 \\ \hline 57 \ 55 \ 51 \ 42 \ 45 \ 57 \ 53 \ 47 \ 44 \\ \hline 25 \ 12 \ 11 \ 10 \ 7 \ 5 \ 10 \ 12 \ 25 \end{array}$$

$$\begin{array}{r} +2.0 \ -0.9 \ -0.6 \ -0.5 \ 0.0 \ -0.6 \ -1.0 \ +2.4 \ +3.0 \ +2.6 \\ \hline 72 \ 101 \ 98 \ 97 \ 92 \ 98 \ 102 \ 68 \ 62 \ 66 \\ \hline 25 \ 14 \ 11 \ 8 \ 7 \ 4 \ 12 \ 17 \ 21 \ 25 \end{array}$$

$$\begin{array}{r} +3.2 \ +3.4 \ -0.6 \ -0.4 \ 0.0 \ 0.0 \ -1.0 \ -0.3 \ +3.0 \ +3.6 \\ \hline 105 \ 108 \ 37 \ 30 \ 26 \ 26 \ 36 \ 24 \ 24 \ 10 \\ \hline 25 \ 13 \ 8 \ 2 \ 3 \ 3 \ 11 \ 14 \ 16 \ 25 \end{array}$$

$$\begin{array}{r} +2.1 \ +1.6 \ -0.5 \ -0.7 \ -0.5 \ 0.0 \ +0.3 \ -0.1 \ -0.7 \ -0.5 \ -0.8 \ +0.8 \\ \hline 54 \ 59 \ 40 \ 32 \ 30 \ 75 \ 76 \ 76 \ 82 \ 80 \ 53 \ 57 \ 48 \\ \hline 25 \ 17 \ 4 \ 6 \ 5 \ 7 \ 5 \ 9 \ 12 \ 13 \ 16 \ 21 \ 27 \end{array}$$

$$\begin{array}{r} -0.3 \ +0.3 \ -0.8 \ 0.0 \ -0.1 \ -1.0 \ -0.9 \ +0.6 \ +1.5 \ +1.8 \\ \hline 52 \ 46 \ 51 \ 49 \ 50 \ 59 \ 58 \ 43 \ 34 \ 31 \\ \hline 25 \ 15 \ 11 \ 8 \ 3 \ 9 \ 14 \ 17 \ 21 \ 25 \end{array}$$

1114 91

215

4.3

10.6

+34 37'-12" N.P. Good.
(Regd. 12" hillside)

3.8

11.1

216

3.0

11.9

217

1.3

13.6

T.P. 9.73 1124 57

0.07

1114.84

218

7.1

17.5

219

3.8

20.8

T.P. 4.95 1128 13

1.39

1123.18

220

4.4

23.5

+25

4.2

23.9

B.M.

4.32

1123.79
1123.81

221

4.7

23.4

38

-1.4	-0.8	-0.9	-0.3	0.0	-0.7	-0.9	+0.8	+1.2
5.7	5.1	5.2	4.6	4.3	5.0	5.2	3.5	3.1
2.5	7.4	7	2		7	7.4	21	2.5

1107.0	1105.1	1105.5	1107.3	1109.7	1107	1111.6	1111.1	1110.5	1110.7	1110.8	1111.0	1108.1	1110.5	
-4.1	-3.0	-2.6	-3.8	-2.3	-1.4	-0.4	-0.1	0.0	-0.6	-0.4	-0.3	-0.1	-3.0	-0.6
7.9	6.8	6.4	7.6	6.1	5.2	4.2	3.9	3.5	4.4	4.2	4.1	3.7	5.9	4.1
5.0	30.6		2.1	2.0	2.4	2	2	2	7	8	7.2	1.5	7.1	2.1

(Regd
open
outlet)

150' Lt

21

16'

Large boulder is placed over each end

-2.0	-1.4	-0.8	-1.2	-0.7	-0.2	+0.1	0.0	-0.6	-0.9	-0.2	-0.6
5.0	4.4	3.8	4.2	3.7	3.2	2.4	3.0	3.6	3.9	3.2	3.6
2.5	7.8	7.5	7.1	7.0	7.3	7.4	7.0	7.6	7.2	7.5	7.5

+1.7	+1.1	-0.7	-1.0	-0.4	+0.1	0.0	+0.1	-0.1	-0.9	+0.9
-0.7	0.2	2.0	2.3	1.7	1.2	1.3	1.3	1.4	2.2	0.4
2.5	7.9	7.4	7.3	7.0	7	7	7	7	15.15	20-2.5

+2.4	+1.9	+0.5	-0.9	-0.4	+0.1	0.0	+0.6	+0.5	+0.3	-0.3	+2.8
6.7	5.2	6.6	8.0	7.5	7.0	7.1	6.5	6.6	6.8	7.4	7.2
2.5	7.2	7.9	7.9	7	7	7	7.8	7.0	7.2	7.2	7.5

+2.1	+1.9	+1.3	-0.2	-0.8	-0.4	0.0	0.0	-0.6	-0.2	-0.4	+0.2	+2.5	+2.9
7.7	7.9	7.5	4.0	4.6	4.2	3.3	3.7	4.2	4.0	3.2	3.6	4.9	5.9
2.5	7.9	7.5	7.1	7.1	7	7	7	7.2	7.0	7.2	7.2	7.9	7.5

+0.4	+0.7	-0.7	-0.1	0.0	-0.5	-0.3	+1.1	+2.5
4.2	3.9	5.3	4.7	4.6	5.1	4.9	3.5	2.1
2.5	1.5	9	9	9	8	7.3	2.5	2.5

some 500
4.2

Tin headed tack in N. root 36" Ash. Lt. opposite Hickox Est.

-0.2	+0.3	+0.1	-0.5	-0.1	0.0	-0.2	-0.5	+0.6	+2.4
4.9	4.4	4.6	5.2	4.9	4.7	4.9	5.2	4.1	2.3
2.5	2.0	7.2	10-6	3	3	3	9	1.4	2.5

1128 13

222

7.0 21.1

223

5

12.0 16.1

T.P.

0.26 1115 47

12.92 1115.21

224

4.2 11.3

+45

5.7 09.8

225

9.6 05.9

+30

10-21-72

11.3 04.2

T.P.

1.21 1103.77

12.91 1102.56

226

5.2 98.6

227

11.6 92.2

T.P.

0.55 1091 30

13.02 1090.75

228

2.9 88.4

229

6.5 84.8

230

9.6 82.2

39

-0.2 +0.4 -0.7 -1.1 0.0 -0.3 -0.5 -0.4 0.0 +2.3

7.2	6.6	7.7	8.1	7.0	7.3	7.5	7.4	7.0	4.7
2.5	7.5	11	7	3	7	10	16	2.5	

+1.1 +1.5 +0.2 -0.7 -1.3 -0.7 0.0 -0.9 -1.3 -0.8 -1.0 +1.4 +2.6

19.9	10.5	11.8	12.7	13.3	12.7	12.8	12.7	13.3	12.8	13.0	10.6	9.4
2.5	1.6	1.3	9	8	5	7	8	10	15	21	3.5	

-0.5 -0.3 -0.2 -0.6 -0.4 0.0 -0.2 -0.4 +0.2 +1.6

4.7	4.5	4.4	4.3	4.6	4.2	4.4	4.6	4.0	2.5
2.5	2.3	1.4	1.2	3	5	7.8	1.9	2.5	

-1.0 -0.3 +0.4 -0.6 0.0 -0.2 +2.1

6.7	6.0	5.3	6.3	5.7	5.9	3.6	General drive
2.5	2.0	1.0	8.7	5	2.5		

0.0 +0.4 +0.6 -0.4 -1.0 -1.4 -0.7 0.0 -0.4 0.0 -1.1 -0.2 +0.7 +2.4

9.6	9.2	9.0	10.0	10.6	11.0	10.3	9.6	1.0	9.6	10.7	9.3	9.9	2.4
2.5	2.1	1.7	1.3	1.1	5	5	5	5	8-14	15	10-17	7.8	2.5

-0.1 +0.4 +0.3 -0.7 -1.6 -0.7 0.0 -0.3 -0.8 -0.4 -0.7 -1.5 -0.3 +2.1 +2.7

11.4	10.7	11.0	11.0	12.9	12.0	11.3	11.5	12.1	11.7	12.0	12.8	11.6	9.2	2.5
2.5	2.0	1.6	1.0	8	5	4	7.8	9	14	15	16	2.2	2.5	

+1.6 -0.5 -0.8 -0.4 0.0 0.0 -0.3 -0.5 -0.1 -0.7 +0.2 +1.5 +4.0

3.6	5.7	6.0	5.6	5.2	5.2	5.3	5.7	5.3	5.7	5.9	3.7	1.2
2.5	1.9	1.5	1.1	1	1	3	7	1.3	1.4	1.5	1.9	2.5

+0.7 -0.5 -0.8 -1.2 -0.4 0.0 -0.1 -0.4 +0.1 -0.3 -1.3 0.0 +2.4

10.7	12.1	12.9	12.8	12.0	11.6	11.7	12.0	11.5	11.9	12.9	11.6	9.2
2.5	1.8	1.3	1.0	9	6	5	6.7	8	1.3	1.4	1.5	2.5

-0.4 0.0 -0.7 -1.0 -0.1 0.0 -0.2 -0.5 -0.1 -0.4 -0.8 0.0 +1.6

3.3	2.7	3.6	3.9	3.0	2.9	3.1	3.1	3.0	3.3	3.7	2.2	1.3
2.5	1.7	1.3	8	2	2.4	6	9	1.4	1.5	1.6	2.5	

-0.7 +0.2 -0.9 -0.7 0.0 0.0 -0.7 -0.4 -0.1 -1.0 -0.2 +1.0

7.2	6.3	7.4	7.3	6.5	7.2	6.9	6.6	7.3	6.7	5.5
2.5	1.4	1.1	5.1	6.3	9	1.8	1.5	1.6-1.9	2.5	

-1.3 -0.4 -0.8 -0.7 0.0 -0.5 -0.9 -0.5 -0.9 -0.5 +0.1

10.4	9.5	9.4	9.8	9.1	9.6	10.0	9.6	10.0	9.6	9.0
2.5	1.0	1.1	1.4	1.4	1.5	1.5	1.4	1.5	1.6	2.5

109130

231 108 80.5

T.P. 1.15 1081 33 111.2 1080.18

232 2.7 78.6

+3.5 3.6 77.7

233 6.4 74.9

234 11.3 70.0

T.P. 0.17 1068 90 12.70 1068.63

235 3.5 65.4

236 4.5 59.4

+3.5 11.8 57.1

T.P. 0.24 1056 36 12.78 1056.12

237 5.4 51.0

+5.0 7.7 48.7

238 9.2 47.2

T.P. 5.24 1050 44 11.6 1045.20

70

-2.4	-0.4	-0.8	-0.6	0.0	-0.3	-0.1	+0.5	-1.3	-0.5	-0.7
13.2	11.2	11.6	11.7	10.8	11.1	10.7	10.3	12.1	11.3	11.5
2.5	1.0	1.4	1.3	1.5	1.8	1.9	1.4	1.5	1.6	2.5

-1.2	-0.4	-0.7	-0.4	0.0	-0.2	-0.7	0.0	-0.5	-1.2	-0.7	0.0	+0.1
3.2	3.1	3.1	3.1	2.7	2.7	3.4	3.7	3.2	3.8	3.4	2.7	2.6
2.5	1.7	1.4	1.4	1.2	1.2	1.7	1.0	1.5	1.7	1.8	2.1	2.5

+0.1	+0.4	-0.2	-0.5	-0.7	-0.3	0.0	+0.2	-0.5	-1.2	-0.7	-0.4	-1.2	-0.8	-0.1	+0.6
3.5	3.2	3.8	4.1	4.0	4.3	3.7	3.6	3.4	4.1	4.3	3.5	4.0	4.3	4.4	3.2
2.5	1.6	1.2	1.4	1.6	1.5	1.4	1.5	1.3	1.7	1.0	1.5	1.6	1.7	1.2	1.7

+1.0	+0.2	-0.4	-0.2	0.0	+0.2	-0.2	-1.0	-0.7	-0.4	-1.3	-0.1	+1.6
5.1	6.8	6.8	6.5	6.4	6.2	6.6	7.4	6.6	6.1	7.7	6.5	4.8
2.5	1.9	1.3	1.5	1.2	1.2	1.6	1.9	1.4	1.4	1.6	1.7	2.5

+1.2	+0.5	-0.4	-0.8	-0.2	0.0	+0.3	-0.5	-0.2	-0.4	-1.4	-0.3	+2.1
11.1	10.8	11.7	12.1	11.5	11.3	11.0	11.8	11.5	11.7	12.7	11.6	12.2
2.5	1.9	1.7	1.6	1.4	1.4	1.2	1.4	1.6	1.4	1.6	1.6	2.5

+1.4	+2.0	+0.2	-0.4	-0.8	-1.1	-0.7	-0.5	0.0	+0.2	-0.7	-0.5	-0.3	-0.7	-1.3	-0.7	+1.9
2.1	1.5	3.3	3.9	4.3	4.6	4.3	4.0	3.8	3.3	3.1	3.0	3.8	4.2	4.8	4.2	1.6
2.5	2.0	1.4	1.0	1.7	1.6	1.5	1.2	1.2	2.4	1.7	1.7	1.0	1.4	1.2	1.7	2.5

+2.2	+0.8	-0.1	-0.8	-1.1	-0.5	0.0	+0.1	-0.3	-0.6	-1.3	-0.5	-0.2	+1.8	+2.5
7.3	8.9	9.6	10.3	10.6	10.0	9.5	9.4	9.8	10.1	10.9	10.0	9.7	9.7	10.2
2.5	2.2	1.7	1.5	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1

+3.1	+1.2	-0.3	-0.7	-0.9	-0.5	0.0	-0.7	-0.5	+0.2	+3.3	+3.4
10.0	12.5	12.5	12.3	11.7	12.5	12.3	11.6	8.5	8.5	8.5	8.5
2.5	1.1	1.3	1.0	1.0	1.1	1.1	1.1	1.1	1.1	1.1	1.1

+5.7	+4.4	+3.6	-0.3	-0.7	-0.4	-0.2	0.0	0.0	-0.3	-0.4	-0.8	-0.1	+1.2	+0.5
3.1	1.8	5.7	6.1	5.8	5.6	5.4	5.4	5.7	5.8	6.2	5.5	4.2	4.2	4.2
2.5	1.1	1.1	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0

+0.2	-0.4	-0.5	-1.0	-0.4	0.0	-0.3	-0.8	-0.5	+0.5	+0.6
7.5	8.1	8.2	8.7	8.1	7.7	8.0	8.5	8.2	7.7	7.1
2.5	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.1

-1.9	-1.3	-0.9	-0.6	0.0	0.0	-0.3	-0.8	-2.3	-3.8
11.1	10.5	10.1	9.8	9.3	9.2	9.5	10.0	11.0	12.0
2.5	1.5	1.5	1.4	1.3	1.3	1.2	1.1	1.1	1.1

1050 44

4.0 46.4

+35 3' x 4 1/2' Stone Box
 Good Cond. Ext. Rt. end
 (Gen. cap over Lt. Box if Reqd)

+80 4.2 46.2

239 3.8 46.6

+50 4.8 47.6

240 4.4 46.0

T.F. 2.19 1043 59 9.04 1041.90

241 2.9 40.7

242 8.0 35.6

243 11.7 31.9

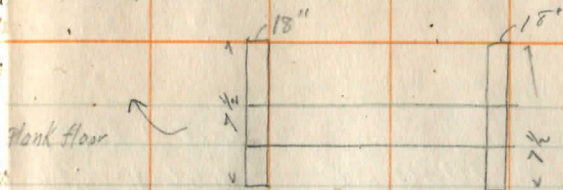
T.P. 2.28 1033 66 12.21 1031.38

B.M. 202 1031.64

244 4.1 29.6

1038.1 1038.2 1038.3 1038.4 1038.5 1038.6 1038.7 1038.8 1038.9 1039.0 1039.1

-8.3	-8.2	-1.0	-0.9	-0.3	+0.1	0.0	-0.1	-1.4	-1.2	-8.2	-7.4	-6.6
12.3	12.5	14	11	10.2	4.2	4	5	5.2	12.2	11.4	10.6	
19	14	14	11	10.2	4.2	4	5	5.2	12.2	11.4	10.6	2.5



x 14'-4" x 16'-4"

-5.8 -4.7 -2.5 -1.8 -0.2 -0.1 +0.2 0.0 0.0 -1.1 -1.4 -0.8 +1.0

10.8 8.9 6.7 6.0 4.4 4.3 4.0 4.2 4.1 5.3 5.2 5.0 3.2

2.5 2.1 1.8 1.5 1.0 2 3.0 4 5 8 15 20 2.5

+3.2 +2.0 +1.9 -0.3 -0.1 -0.3 +0.1 0.0 -0.1 -0.4 -0.3 +1.2 +6.7

0.5 1.2 1.7 1.1 3.7 4.1 3.7 2.7 2.7 4.2 4 2.6 -2.9 Level

2.5 2.2 1.7 1.2 4 5 3 2 2 4.2 1.4 1.4 2.5

+1.5 +1.8 +1.4 -0.4 0.0 0.0 +0.1 +0.9 +1.7 +4.1

1.3 1.0 1.4 1.1 3.3 3.8 3.7 2.7 2.7 4.2 4 2.6 -2.9

2.5 2.0 1.6 1.2 4 5 3 2 2 4.2 1.4 1.4 2.5

+1.3 +1.0 +0.8 -0.2 -0.1 -0.4 0.0 -0.3 +0.3 -0.2 +0.2 +0.7 +2.7 +3.2

3.1 3.4 3.5 4.5 4.5 4.3 4.4 4.7 4.1 4.6 4.3 3.7 4.2 4.2

2.5 2.0 1.5 1.2 1.0 4 4 4 4 11 13 13 12 2.5

+1.2 +1.1 -0.2 -0.1 -0.7 0.0 0.0 -0.9 +0.1 -0.4 +1.7 +2.1

1.7 1.8 3.1 3.0 3.5 2.9 2.9 3.7 2.8 2.3 1.5 0.8

2.5 2.1 1.3 4 4 2 2 11 13 2.0 2.5

+1.0 +0.7 -0.3 -0.8 -0.1 -0.4 0.0 -0.1 -0.3 +0.5 -0.3 +1.5 +1.8

2.0 1.3 8.3 8.8 8.1 8.1 8.0 8.1 8.3 7.5 8.3 6.5 6.2

2.5 2.0 1.6 1.3 1.1 1.0 2 2 2 12 15 2.0 2.5

+0.5 +0.4 -0.5 -0.2 +0.1 0.0 -0.3 +0.3 +0.6 +0.3 +0.8 +1.9

11.2 11.3 11.5 11.3 11.5 11.7 12.0 11.4 11.1 11.4 10.9 9.8

2.5 1.6 1.5 1.1 1.3 1.4 1.4 1.4 1.4 1.6 1.6 2.5

Tin headed tack W. root 15" Maple 243+60, 28' Rt

0.0	-0.5	0.0	-0.1	+0.3	0.0	-0.2	+0.2	+0.1	-0.3	+0.2	+1.1
4.1	4.6	4.1	4.2	3.8	4.1	4.3	3.9	4.0	4.4	3.9	3.1
2.5	1.9	1.2	1.2	1.5	3	4	6	13	1.4	1.6	2.5

1028 ²15

252+76 2 1/2' x 4' Stone Box

Very Good Cond. Ext. Lt. end
1 1/2' dirt in bottom clearcut 100' Lt.

4.6 23.6

253.

4.1 24.1

254

1.8 26.3

T.F. 11.67 1039 17

0.65 1027.50

255

8.2 31.0

256

2.5 36.7

T.F. 6.16 1043 44

1.89 1037.28

257

4.7 38.7

+30

4.2 39.2

258

5.2 38.2

259

7.9 35.5

260

8.3 35.1

+59 6" tile

Repd. 12" Pipe

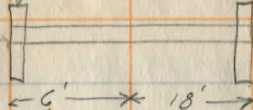
8.0 35.4

✓

1017.5 -6.1 1016.7 -4.9 1018.5 -5.1 1020.0 +0.2 1023.0 +0.6 1024.2 +0.3 1025.4 +0.0 1026.9 +0.3 1028.7 +0.5

2.5' from parapet to top of opening

2.6' from par. to top of opening



-1.1 -1.2 -0.2 0.0 +0.4 0.0 +0.1 -1.0 -1.3 -2.3
5.2 5.3 4.3 4.1 3.7 4.1 4.0 5.1 5.4 6.4
25 2 3 5 7 7 12 15 21 25

+1.2 +1.0 +0.4 0.0 0.0 +0.3 0.0 -0.3 +2.2 +2.5
0.7 0.9 1.5 1.9 1.9 1.6 1.9 2.2 -0.3 -0.6
25 20 2 4 4 13 13 14.15 20 25

+2.5 +2.0 -0.8 0.0 -0.4 0.0 0.0 -0.2 -0.1 +2.2 +2.3
5.7 6.2 9.0 8.2 8.6 8.2 8.2 8.4 8.3 6.0 5.9
25 17 11 7 3 2 5 13 19 25

+0.5 +0.3 -0.6 0.0 -0.3 -0.1 -0.4 +1.0 +1.8
2.0 2.2 3.1 2.5 2.1 2.6 2.7 1.5 0.7
25 14 12 7 7 11 12.4 17 25

-0.9 -0.2 -0.7 -0.2 0.0 +0.1 -0.1 +1.0 +1.8
5.6 4.9 5.4 4.9 4.7 4.6 4.8 3.7 3.9
25 17 13 10 8 10 14 12 12

-1.4 -1.7 -1.1 -0.4 -0.8 -0.5 0.0 -0.3 -0.1 +0.5 +1.1 +1.4
5.6 5.9 5.3 4.6 5.9 4.7 4.2 4.5 4.3 3.7 3.1 3.8
25 22 21 17 13 10 8 4 11 18 21 25

-0.7 -0.4 +0.3 -0.2 -0.6 0.0 0.0 -0.5 -0.4 +0.9 +1.5
5.4 5.6 4.9 5.4 5.2 5.2 5.2 5.7 5.6 4.3 3.7
25 20 12 13 10 9 9 9 13 16 25

-0.4 -0.1 +0.6 +0.3 -0.2 0.0 +0.1 -0.1 +0.2 -0.1 +1.1 +2.8 +2.5
8.3 8.0 7.3 7.6 7.1 7.9 7.8 8.0 7.7 8.0 6.8 5.1 5.4
25 19 15 9 8 9 9 11 12 14 21 25

-1.8 -0.8 -0.7 -0.2 0.0 +0.3 0.0 -0.3 +0.2
10.1 2.1 9.0 8.3 8.0 8.3 8.0 8.2 8.1
25 15 8 5 5 10 14 20 25

-2.4 -1.9 -1.0 -0.5 0.0 +0.1 0.0 -1.1 -0.6 -0.5
10.4 9.9 9.0 8.5 8.9 7.9 8.0 9.1 8.6 8.5
27 10 9 5 4 11 13 14 15 25

about 3' show
make 90°



1043 44

261

9.P. Sat. P.M.

T.P. 6.94

1043 80

8.5 34.9

6.58 1036.86

262

10.24.22

8.5 35.3

263

7.8 36.0

264

5.1 38.7

+25

4.0 39.8

+50

4.0 39.8

265

5.8 38.0

+85

8.6 35.2

266

9.1 34.7

T.P. 2.20 10.34 63

11.45 1032.35

267

2.2 32.4

268

5.1 29.5

269

5.0 26.4

44

-0.9	-1.0	-0.4	-0.6	-0.1	0.0	+0.2	-0.3	+0.2	-0.4	-0.2
$\frac{24}{25}$	$\frac{35}{19}$	$\frac{82}{13}$	$\frac{21}{7}$	$\frac{25}{5}$	$\frac{85}{4}$	$\frac{83}{5}$	$\frac{88}{11}$	$\frac{83}{14}$	$\frac{89}{14}$	$\frac{87}{25}$

spike in top - Lt.	+0.3	-0.2	-0.4	0.0	0.0	-0.4	-0.2	-0.3	0.0
	$\frac{82}{25}$	$\frac{87}{9}$	$\frac{82}{7}$	$\frac{85}{5}$	$\frac{87}{10}$	$\frac{87}{14}$	$\frac{83}{12}$	$\frac{83}{12}$	$\frac{85}{25}$

+2.2	+1.2	+0.6	-0.1	0.0	+0.1	-0.1	+0.9	+1.3	+1.2
$\frac{56}{25}$	$\frac{66}{18}$	$\frac{72}{10}$	$\frac{79}{7}$	$\frac{72}{7}$	$\frac{77}{5}$	$\frac{79}{12}$	$\frac{67}{15}$	$\frac{65}{18}$	$\frac{66}{25}$

+2.6	+1.4	-0.2	0.0	+0.1	-0.2	+1.1	+1.0	+1.2
$\frac{25}{25}$	$\frac{37}{15}$	$\frac{53}{6}$	$\frac{51}{6}$	$\frac{50}{8}$	$\frac{53}{11}$	$\frac{40}{12}$	$\frac{41}{18}$	$\frac{32}{25}$

+2.6	+1.2	+0.8	-0.3	0.0	+0.1	-0.3	-0.5	+0.5	-0.4
$\frac{14}{25}$	$\frac{28}{20}$	$\frac{32}{12}$	$\frac{43}{6}$	$\frac{40}{6}$	$\frac{37}{5}$	$\frac{43}{11}$	$\frac{43}{12}$	$\frac{35}{12}$	$\frac{44}{25}$

+2.1	+0.8	-0.2	0.0	+0.2	-0.2	-0.4	+0.1	-0.1
$\frac{19}{25}$	$\frac{32}{13}$	$\frac{42}{6}$	$\frac{45}{6}$	$\frac{37}{3}$	$\frac{42}{5}$	$\frac{41}{11}$	$\frac{38}{12}$	$\frac{41}{25}$

+3.5	+1.5	-0.2	0.0	+0.1	-0.3	0.0	+0.8	+1.2	+0.6
$\frac{23}{25}$	$\frac{43}{17}$	$\frac{65}{5}$	$\frac{58}{5}$	$\frac{51}{5}$	$\frac{61}{6}$	$\frac{58}{10}$	$\frac{59}{12}$	$\frac{46}{18}$	$\frac{52}{25}$

+2.0	+0.5	-0.4	0.0	0.0	-0.2	+0.8	+0.9	+0.6
$\frac{66}{25}$	$\frac{81}{12}$	$\frac{90}{8}$	$\frac{80}{8}$	$\frac{80}{4}$	$\frac{83}{10}$	$\frac{73}{13}$	$\frac{77}{12}$	$\frac{80}{25}$

-3.0	-2.5	-0.5	0.0	0.0	+0.2	-0.2	-0.1	+0.5	+0.6	+0.7
$\frac{124}{25}$	$\frac{116}{17}$	$\frac{36}{11}$	$\frac{21}{5}$	$\frac{21}{5}$	$\frac{89}{3}$	$\frac{83}{5}$	$\frac{92}{10}$	$\frac{15}{13}$	$\frac{80}{12}$	$\frac{81}{25}$

+0.5	0.0	-0.2	0.0	+0.1	-0.4	-0.2	+0.1	-0.6
$\frac{17}{25}$	$\frac{32}{10}$	$\frac{32}{5}$	$\frac{23}{5}$	$\frac{21}{3}$	$\frac{26}{10}$	$\frac{28}{14}$	$\frac{21}{12}$	$\frac{22}{25}$

+1.3	+1.2	+0.6	-0.2	0.0	+0.1	-0.2	-0.3	+0.7	+1.6
$\frac{38}{25}$	$\frac{39}{13}$	$\frac{45}{9}$	$\frac{57}{4}$	$\frac{51}{4}$	$\frac{50}{13}$	$\frac{54}{4}$	$\frac{44}{13}$	$\frac{44}{14}$	$\frac{35}{25}$

+1.8	+1.5	+0.3	+0.5	-0.1	-0.4	0.0	-0.1	-0.7	-0.3	+1.2	+2.1
$\frac{43}{25}$	$\frac{49}{22}$	$\frac{27}{18}$	$\frac{28}{14}$	$\frac{19}{11}$	$\frac{26}{11}$	$\frac{80}{11}$	$\frac{21}{5}$	$\frac{24}{7}$	$\frac{63}{11}$	$\frac{63}{15}$	$\frac{54}{25}$

1034, 63

T.P.	298	1027	14	10.47	1024.16
					1026.03
J.M.	110	1027	13	1.10	1026.01
270				3.3	23.8
+ 2.84				3.9	23.2
				3.3	23.8
				4.2	22.9
				6.5	20.6
				3.4	23.7
				3.1	24.0
				3.7	23.7
				4.1	23.0
270+60				4.6	22.5
170				4.4	22.7
271				7.3	19.8
+50				10.9	16.2
T.P.	1.49	1016	23	12.39	1014.74
272				5.5	10.7
				8.15	1008.08
T.P.	0.01	1013	5	12.72	1003.51

45

Tin headed tack E. root 30" Nape 30' Lt. 269+92

	+0.3	+0.6	+1.5	+1.9	0.0	0.0	+0.9	+0.3	0.0	+0.3	+1.3
Rt. 7	$\frac{30}{25}$	$\frac{27}{20}$	$\frac{18}{13}$	$\frac{16}{5}$	$\frac{33}{4}$	$\frac{33}{7}$	$\frac{29}{13}$	$\frac{33}{17}$	$\frac{28}{21}$	$\frac{30}{25}$	2 Lt

2. Rd

Take Lt stick water to Lt.

30' Lt on END

100' " " " "

200' " " " "

50' Rt. " " "

Take

150' " " " "

200' " " " "

+0.4 -0.4 -0.1 -0.3 0.0 +0.2 +0.9 +0.6

$\frac{12}{25}$	$\frac{50}{21}$	$\frac{47}{17}$	$\frac{19}{13}$	$\frac{46}{7}$	$\frac{42}{7}$	$\frac{37}{7}$	$\frac{40}{12-25}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	--------------------

+0.1 -0.4 -0.8 -0.4 +0.1 0.0 -0.1 +0.5 +0.2 +0.8 +0.2

$\frac{12}{25}$	$\frac{28}{18}$	$\frac{52}{14}$	$\frac{18}{7}$	$\frac{43}{7}$	$\frac{24}{7}$	$\frac{45}{10}$	$\frac{37}{14}$	$\frac{42}{19}$	$\frac{35}{25}$
-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

+2.3

50 +2.3 +1.7 +0.6 0.0 -0.6 +0.1 0.0 -0.6 -0.2 +2.2 +2.3 +2.6

$\frac{50}{25}$	$\frac{41}{20}$	$\frac{52}{15}$	$\frac{67}{14}$	$\frac{73}{10-8}$	$\frac{71}{7}$	$\frac{72}{5}$	$\frac{23}{8}$	$\frac{75}{7}$	$\frac{51}{16}$	$\frac{50}{13}$	$\frac{47}{25}$
-----------------	-----------------	-----------------	-----------------	-------------------	----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------

+1.2 +1.6 +1.9 -0.3 -0.4 +0.2 0.0 -0.5 -0.3 +1.4 +4.1 +4.7

$\frac{17}{25}$	$\frac{13}{22}$	$\frac{20}{17}$	$\frac{11}{12}$	$\frac{113}{8}$	$\frac{101}{3}$	$\frac{107}{6}$	$\frac{114}{9}$	$\frac{112}{12}$	$\frac{93}{20}$	$\frac{68}{25}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	-----------------	-----------------

-0.2 +0.4 -0.5 -0.7 +0.1 0.0 +0.3 +0.1 +0.8 +3.8 +4.8

$\frac{57}{25}$	$\frac{51}{23-20}$	$\frac{60}{17-18}$	$\frac{62}{11}$	$\frac{54}{5}$	$\frac{55}{5}$	$\frac{52}{6}$	$\frac{54}{11}$	$\frac{41}{13}$	$\frac{17}{20}$	$\frac{07}{25}$
-----------------	--------------------	--------------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

56 Cor Watering Trough

Prospective Drainage

BM. 2.44 1306.65

1304.21

53+20

5.6 01.1 0

4.9 01.8 50'

5.0 01.7 100'

€ 6.3 00.4 200'

7.3 99.4 300

8.5 98.2 300+2

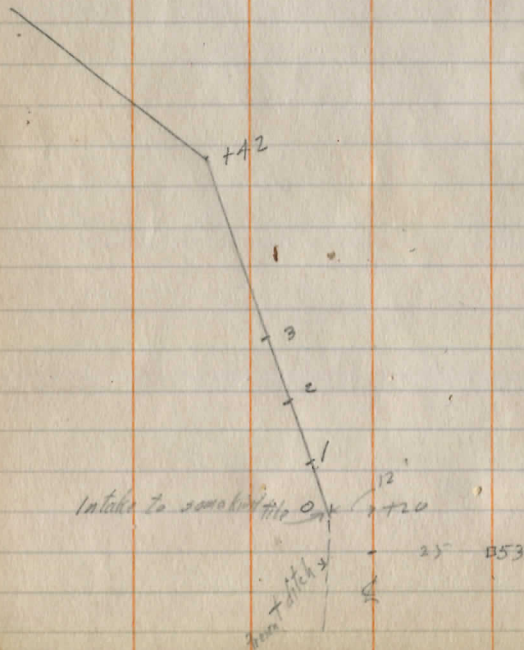
9.7 97.0 400

T.P. 397 1301.82

7.9 1298.75 500

8.7 93.1 500

11.9 89.9 600 To fence & pasture lot



12.12	966.05		953.95	
12.10	977.91	0.24	965.81	
		8.73	969.18	
12.32	989.09	1.14	976.77	973.25
		8.74	980.35	973.85
		5.1	984.0	978.50
		1.82	987.27	980.77
Geauga Co. 275+00		2.2	986.9	
11.18	1000.22	0.05	989.04	
		4.07	996.15	
274+00		6.3	993.9	
11.78	1011.43	0.57	999.65	
273		9.6	1001.8	
272		0.6	1010.8	

July 14, 1926.

Marks - Canfield. 48

Lake Co. B.M. #36 spike in root 30" Elm
183+60 - 16' L. of \pm ,

Lake Co. B.M. E.M., Corners + 150' \pm , Right
Stake, 187+50, Marked 3'5" \downarrow
" 189+00 " 6'6" \downarrow
" 188+50 " 5'6" \downarrow
" 189 " 6'6" \downarrow
 \pm Road,

(E1. 996.06) Geauga Co. Survey 30" Elm
B.M. Left of Sta. 274+10, Spike, S.E. Root

	9.10	957.00		947.90
183				
183			7.1	949.9
	2.25	950.15	9.10	947.90
182			7.0	943.2
	1.08	939.57	11.66	938.49
181			4.8	934.8
180+50			13.2	926.4
	3.03	930.54	12.06	927.57
			7.32	923.22
180			12.6	917.9
	0.73	919.34	11.93	918.61
179+90			11.0	918.3
	5.86	915.48	7.72	909.62
179+70			10.2	905.3
179+50			12.2	903.3
179			1.69	913.79
	10.87	924.66		
	12.27	936.23	0.70	923.96
178+50			7.2	929.0

Stake

June 7, 1927, Marks - D. Parks - R. Hassel⁴⁹

B.M. spike in R.P. intwin Cherry, Back of Swings ^{in school Yard}

4.2	3.9	4.1	8.3	7.5	7.1	7.0	7.2	1.0	0.5	0.0
4.0	2.8	4.8	14	11	0	7.5	10	20	30	48

4.2	4.2	8.5	7.6	6.7	6.6	7.0	5.7	1.5	1.0	1.5
4.5	3.5	2.6	2.4	1.3	2	0	3	11	32	40

10.5	4.2	5.9	5.2	5.7	5.2	4.8
4.5	3.8	3.1	2.6	6	4	3
						0

T.P. Top of stake, 180+50

X on W. Corner, S. Ret. Wall (923.25 rec)

T.P. Top of stake, 180+50

12.2	12.2	6.0
7.0	0	60
Right End 20 Arch		

Top of stake

12.0	10.3	9.5	8.0	7.0	6.2
7.0	5.0	4.2	3.3	2.3	0
					5.1
					60

936.23

178+00 2.8 933.4

11.91 947.74 0.40 935.83

177+56 6.0 941.7

11.95 959.19 0.50 947.24

177 10.2 949.0

176+50 2.9 956.3

11.38 969.81 0.76 958.43

176+50

176 7.2 962.06

10.53 976.74 3.60 966.21

176

$$\frac{50}{0.39} \frac{4.0}{35} \frac{2.6}{33} \frac{3.2}{33} \frac{2.7}{30.5} \frac{3.1}{7.5} \frac{4.5}{6} \frac{3.0}{5} \frac{2.8}{0} \frac{1.9}{50} \frac{3.0}{60}$$

$$\frac{2.7}{50} \frac{3.2}{45} \frac{5.0}{37} \frac{6.6}{8} \frac{8.3}{3.5} \frac{7.5}{2} \frac{6.0}{0} \frac{2.8}{5} \frac{4.5}{27} \frac{0.0}{70} \frac{+3.0}{50}$$

$$\frac{4.5}{50} \frac{5.0}{35} \frac{9.5}{30} \frac{8.4}{25} \frac{9.0}{1} \frac{10.2}{0} \frac{5.7}{6} \frac{0.0}{60}$$

$$\frac{0.0}{24} \frac{2.3}{19} \frac{3.3}{17} \frac{2.3}{15} \frac{2.9}{0} \frac{3.0}{7} \frac{3.7}{9} \frac{2.1}{12}$$

$$\frac{5.9}{50} \frac{5.3}{31.5} \frac{8.3}{15} \frac{7.6}{35} \frac{5.1}{50}$$

$$\frac{1.8}{21} \frac{6.2}{10} \frac{7.8}{7} \frac{7.0}{6} \frac{7.2}{0} \frac{7.5}{7} \frac{9.2}{9.5} \frac{7.3}{16} \frac{0.2}{25}$$

$$\frac{0.5}{50} \frac{4.7}{28} \frac{6.6}{35} \frac{5.8}{50}$$

181 1.1 935.9 934.8

1.2 927.1 10.0 925.9

181

180+50 0.8 927.2 926.4

180 1.0 918.9 917.9

179 5.4 919.2 913.8

$\frac{1.1}{0}$ $\frac{1.4}{9}$ $\frac{10.0}{22}$

$\frac{6.9}{31}$ $\frac{9.0}{35}$ $\frac{12.7}{60}$

$\frac{0.8}{0}$ $\frac{11.0}{17}$ $\frac{13.0}{50}$
Cr. Bank

$\frac{1.0}{0}$ $\frac{9.3}{12}$ $\frac{13.1}{16}$ $\frac{14.5}{20}$ $\frac{12.9}{44}$ $\frac{12.9}{50}$

$\frac{10.0}{Ret. Wall.}$ $\frac{5.4}{0}$ $\frac{2.9}{6}$ $\frac{5.2}{26}$ $\frac{5.8}{50}$ $\frac{1.2}{60}$

July 28, 1927 Marks, D. Parks, Hassel⁵²

2.68 916.47

913.79

6.47 910.00

Top of stake, Sta. 179+00

Elevation Points Set.

Culverts

108+90
B.M. 9.58 1210.76 1201.18

120+70
1.25 1181.50 1180.25

146+35 5.22 1093.72 1088.50
7.82 1085.90

152+25 6.3 1094.3 1088.0

168+40 6.30 1127.24 1022.94

177+

May 17, 1928
Showers, W.C. Marks-D. Parks-C. Rand

Right of 114+90

1206.2 4.56 $\frac{C1.0}{30}$ 1205.3 5.46 $\frac{C2.0}{30}$

May 18, 1928, Marks-Parks-Rand.

Slope Hub, Right 120+00
1173.9 7.6 $\frac{C6.0}{30}$ 1171.6 9.90 $\frac{C3.0}{30}$

Right Slope Hub, 146+00
inlet of 6" Drain Tile, 16' Right

1086.60 7.12 $\frac{C2.0}{30}$ 1085.70 $\frac{C3.0}{30}$
Right Slope Hub, 152+00

1087.3 7.0 $\frac{C1.0}{30}$ $\frac{C2.0}{30}$ 7.9 1086.4
May 28, 1928 Marks, Parks, Rand + Hassel

Bottom of S.E. corner boards, House Left, 169+15

1120.91 8.33 $\frac{C1.0}{30}$ 1121.59 7.65 $\frac{C3.0}{30}$

18" Hillside Culvert, 100' long.
Grades set to fit ground.

Warm Sun

June 11, 1928 D. Parks, R. Hassel, C. Rand

N.E. Side

S.W. Side

Tin-headed Tack, N.E. Root 12 Maple, ^{30'} _{51.5'}

B.M. 5.77 1009.80 1009.03

195,760

1004.00 $\frac{8.30}{5.80}$ $\frac{C3.5}{30}$ 1000.25 $\frac{7.65}{9.15}$ $\frac{C1.5}{30}$

N.E. Side

S.W. Side

Tin-headed Tack, W Root 10' Maple R. Fr. _{0.75}

B.M. 2.87 1096.68 1093.81

209,194

N.E. 1087.11 $\frac{6.57}{9.57}$ $\frac{C3.0}{30}$ 1086.99 $\frac{8.29}{10.29}$ $\frac{C2.0}{30}$

Warm Sun Wind

June 13, 1928 D. Parks, R. Hassel, C. Rand

N.E. Side

S.W. Side

Slope Stake Rt. Sta 210 $\frac{7.51}{8.71}$ $\frac{C3.0}{35}$ 1107.30 $\frac{9.51}{8.5}$ $\frac{C2.0}{35}$

5.16 1116.81 1111.65

215,145

1108.10 $\frac{8.71}{9.71}$ $\frac{C3.0}{35}$ 1107.30 $\frac{9.51}{8.5}$ $\frac{C2.0}{35}$

N.E. Side

Tin-headed Tack, N. Root, 26" Ash L opposite Hitchcock Est.

B.M. 1.58 1125.37 1123.79

1115.90 $\frac{5.97}{9.77}$ $\frac{C3.5}{10 FT to Pipe}$

216,190 - 218+10 side Road Culvert

1111.70 $\frac{11.67}{13.27}$ $\frac{C2.0}{10 FT to Pipe}$

238+35 Concrete Extension to culvert
Headwall stakes on both sides.

247+20 Concrete Extension to culvert
Headwall stakes on both sides

252+76 Concrete Extension to culvert
Headwall stakes on both sides

5.11 114.11 1136.00
260+60

B.M. 1.51 1027.54 1026.03
269+93 Inlet, 1.84
270+60 Manhole 3.54
271+30 Outlet. 4.84

N.E. side

S.W. side

Slope Hub R Sta 261
1032.77 $\frac{6.34}{8.34}$ $\frac{CB, 0}{30}$ 1033.73 $\frac{1.88}{7.38}$ $\frac{CB, 5}{30}$

June 29, 1928 Marks, Parks, Rand, Hassel

B.B., Left, 269+92.
1022.7 4.84 Cut 3.0 Stake 5' Right
1020.01 7.54 Cut 4.0 do
1014.7 12.84 Cut 8.0 do

B.M. 486 1128, 657123, 79

216+90-218+10 Side road culvert reset

1st Culvert N.W. of Chardon - Center on

4.4
<u>1.7</u>
6.1
8.55
9.20

Cloudy Windy

June 30, 1928 D. Parks, C. Road 17 Has
N.E. 57th
7th Headed Tack, N root 36" Ash Opposite
Wildcock Est.

1115.90 ^{8.75} ^{0.40} 12.70 10 ft to end of pipe

1111.70 ^{13.95} ^{0.30} 16.95 10 ft to end of pipe

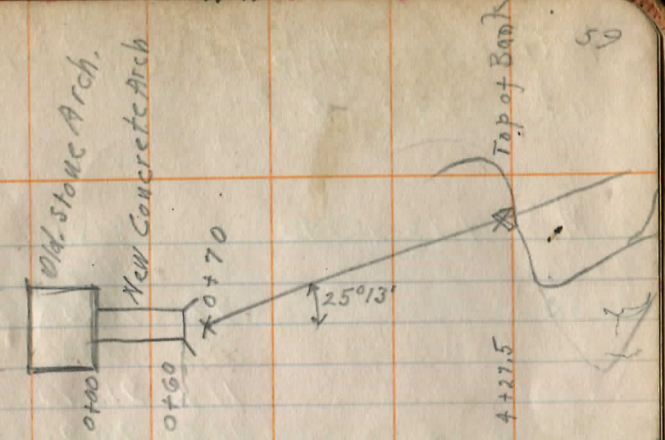
Chardon - Mentor - Road,
June 17, 1929 - Marks + Huckley
Fair, Warm;

Sump, Diedrichs Cellar Floor
Fh. Inlet, 15" Vit. Pipe Culvert.
" " Out let, " " " "

Lay 2 1/4" Corr. Pipe, making F.L. 9" lower
than F.L. of 15" Vit. Pipe

Sept. 19, 1927 Marks-D. Parks, Rand.

	6.12	924.42		918.30
5+00				916.0
4+50				915.5
4	13.30	931.60		918.30
3+50				915.0
3				914.5
2+50				914.0
2	0.18	919.64	12.12	919.48
1+50				912.0
1				911.0
0+70			9.65	910.01
				907.0
				904.0



B. M., Left of 4+50

	0		
	$\frac{C 3.5}{9.5}$	$\frac{C 3.9}{0}$	$\frac{C 4.0}{10.0}$
	$\frac{C 12.5}{18.5}$	$\frac{C 12.6}{0}$	$\frac{C 12.2}{18.2}$
	$\frac{C 10.4}{16.4}$	$\frac{C 10.8}{0}$	$\frac{C 10.9}{16.9}$
	$\frac{C 6.3}{12.3}$	$\frac{C 6.9}{0}$	$\frac{C 7.8}{13.8}$
	$\frac{C 5.5}{11.5}$	$\frac{C 5.5}{0}$	$\frac{C 5.7}{11.7}$
	$\frac{C 5.2}{11.2}$	$\frac{C 5.2}{0}$	$\frac{C 5.2}{11.2}$
	$\frac{C 4.4}{10.4}$	$\frac{C 5.0}{0}$	$\frac{C 5.5}{11.5}$
Rec. 910.00	$\frac{C 4.5}{10.5}$	$\frac{C 4.9}{0}$	$\frac{C 6.8}{12.8}$
		$\frac{C 5.9}{0}$	

Stake on Walnut Tree, N. of Culvert

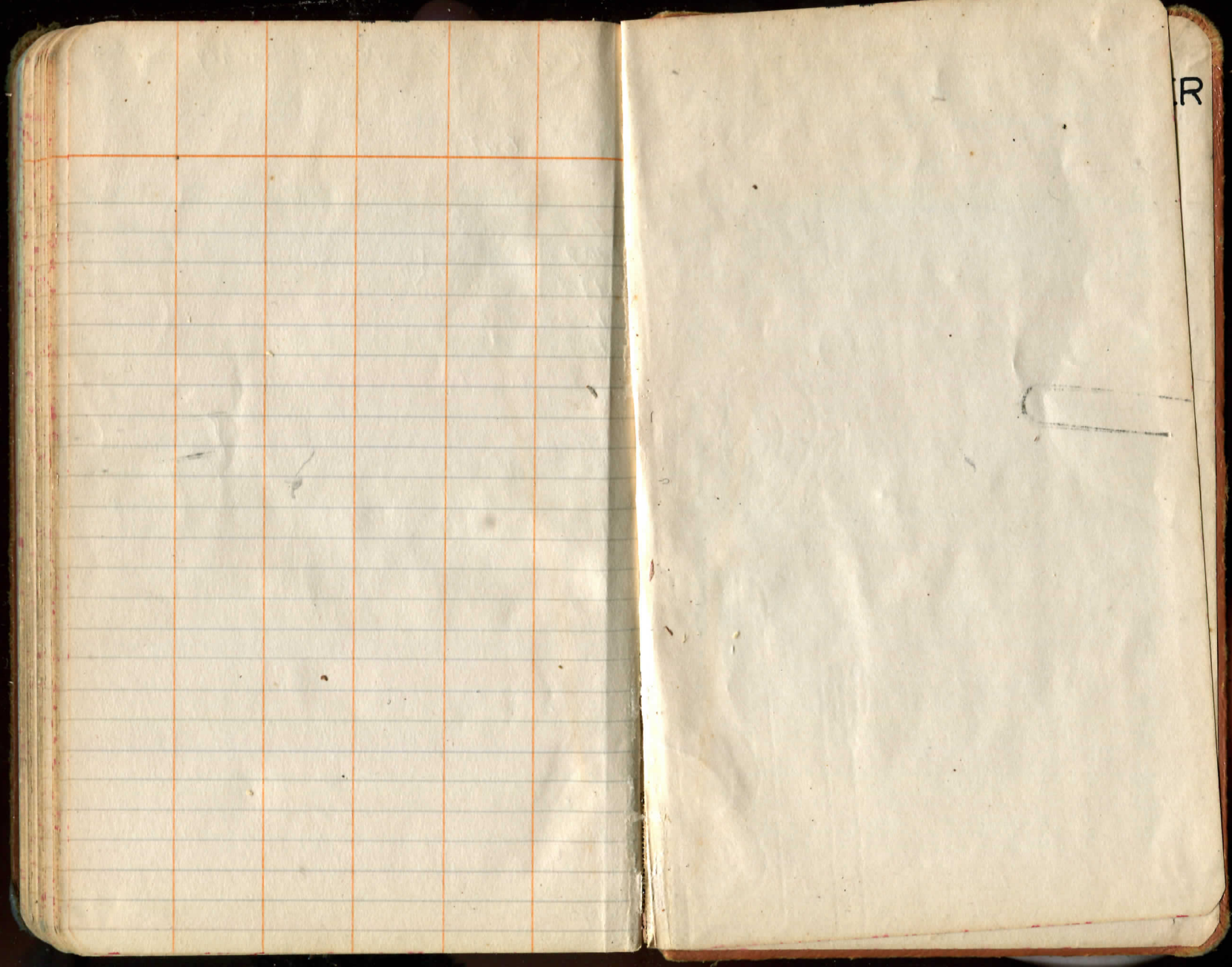
Grades, Inlet to Culvert
at 179+45.7

B. M.	7.15	92545	918.30	Grade
4+00	8.8	91665	915.00	
3+50	9.9	91555	914.50	
3	10.9	91455	914.0	
2+50	11.7	91375	913.0	
2	12.5	91295	912.0	
1+50			911.0	

Nov. 15, 1927 Marks, Richey 60

Grade
Rod Cut,

10.45	1.6
10.95	1.0
11.45	0.5
12.45	0.7
13.45	0.9



R

153.87
 461515
 617.02

PLEASE RETURN TO
 GAUGA COUNTY ENGINEER

COURT HOUSE
 CHARDON, O.
 PHONE 250-X

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	16.50.0
19	3.13.6	39	6.43.6	59	9.73.6	79	12.87.0	99	16.17.0
18	2.97.0	38	6.27.0	58	9.57.0	78	12.70.6	98	16.00.6
17	2.80.6	37	6.10.6	57	9.40.6	77	12.54.0	97	15.84.0
16	2.64.0	36	5.94.0	56	9.24.0	76	12.37.6	96	15.67.6
15	2.47.6	35	5.77.6	55	9.07.6	75	12.21.0	95	15.51.0
14	2.31.0	34	5.61.0	54	8.91.0	74	12.04.6	94	15.34.6
13	2.14.6	33	5.44.6	53	8.74.6	73	11.88.0	93	15.18.0
12	1.98.0	32	5.28.0	52	8.58.0	72	11.71.6	92	15.01.6
11	1.81.6	31	5.11.6	51	8.41.6	71	11.55.0	91	14.85.0
10	1.65.0	30	4.95.0	50	8.25.0	70	11.38.6	90	14.68.6
9	1.48.6	29	4.78.6	49	8.08.6	69	11.22.0	89	14.52.0
8	1.32.0	28	4.62.0	48	7.92.0	68	11.05.6	88	14.35.6
7	1.15.6	27	4.45.6	47	7.75.6	67	10.89.0	87	14.19.0
6	1.00.0	26	4.29.0	46	7.59.0	66	10.72.6	86	14.02.6
5	88.6	25	4.12.6	45	7.42.0	65	10.56.0	85	13.86.0
4	72.0	24	3.96.0	44	7.26.0	64	10.39.6	84	13.69.6
3	55.6	23	3.79.6	43	7.09.6	63	10.23.0	83	13.53.0
2	39.0	22	3.63.0	42	6.93.0	62	10.06.6 in.	82	13.36.6 in.
1	22.6 in.	21	3.46.6 in.	41	6.76.6 in.	61	9.90.0	81	13.20.0

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

